Hot \& Cold Water Piping Systems made of Polypropylene

## IECHNICAL MANUAL POLO-ECOSAN



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## General Information

The information provided in this technical manual is intended to help you select our products for your application. Text and images were compiled with utmost care. Nevertheless, errors cannot be entirely excluded. POLOPLAST does not assume legal liability or any other form of liability for erroneous information and its consequences. POLOPLAST is grateful for any suggestions or comments.

### 1.1 POLO-ECOSAN Installation System

The POLO-ECOSAN installation system consists of various pipes designed for various fields of application and guarantees a flawless supply of the most precious of all comestibles: drinking water.

## Connection Technique using Heated-Tool Socket Welding

When the pipe and the fitting are welded, their plastic materials fuse together to form a homogeneous, firmly bonded whole. Special tools are used to heat up pipe and fitting, which are then just joined together. This connection is reliable and lastingly leakproof.

### 1.1.1 System Components

### 1.1.1.1 Fittings

The PP-R-metal connection of the POLO-ECOSAN fittings excels by its leakproofness and resistance to torsion. This connection withstands decades of operational loads without any difficulty. Thanks to the specific geometry of their inserts, which are made of high-grade brass, the moulded parts meet the highest safety standards and guarantee safe laying.


The metal threads of the POLOPLAST brass components meet the requirements of the DIN EN 10226 standard and are manufactured from high-quality brass. Moreover, the material complies with the current version of the recommendations (as at 2014) of the Federal Environment Agency on "Materials suitable from a drinking water hygiene point of view". This guarantees that the limit values of the "Deutsche Trinkwasserverordnung (TrinkwV 2001)" (German Drinking Water Ordinance) are reliably observed. All POLO-ECOSAN fittings are compatible with all POLO-ECOSAN pipes (refer to page 8 and following).

### 1.1.1.2 Pipes and Fittings

All pipes and fittings of the POLO-ECOSAN installation system are made of PP-R, with only high-quality raw materials being used. This raw material is equipped with high-grade stabilizers. The stabilizer package protects the polymer from oxidation, which may occur, for example, following long-term exposure to high temperatures $>70^{\circ} \mathrm{C}$ and high pressure.

### 1.1.2 Material-related Guide Values of PP-R

| Properties | Measuring method | Unit | Value |
| :---: | :---: | :---: | :---: |
| Density | ISO 1183 | $\mathrm{~kg} / \mathrm{m}^{3}$ | 898 |
| Melt Flow Rate $230^{\circ} \mathrm{C} / 2.16 \mathrm{~kg}$ | ISO 1133 | $\mathrm{~g} / 10 \mathrm{~min}$. | 0.3 |
| Modulus of Elasticity in Tension $(1 \mathrm{~mm} / \mathrm{min})$ | ISO 527 | MPa | 900 |
| Tensile Stress at Yield $(50 \mathrm{~mm} / \mathrm{min})$ | ISO 527 | Mpa | 28 |
| Charpy Impact Strength, notched $\left(+23^{\circ} \mathrm{C}\right)$ | ISO 179 | $\mathrm{~kJ} / \mathrm{m}^{2}$ | 25 |
| Coefficient of linear expansion | DIN 53752 | $\mathrm{~mm} / \mathrm{mK}$ | 0.15 |
| Thermal conductivity | DIN 52612 | $\mathrm{~W} / \mathrm{mK}$ | 0.24 |
| Pipe surface roughness K |  | mm | 0.007 |
| Specific heat at $20^{\circ} \mathrm{C}$ | Calorimeter | $\mathrm{KJ} / \mathrm{kg} \mathrm{K}$ | 2.0 |

## SYSTEM DESCRIPTION

### 1.1.3 Material-related Guide Values of PP-RCT

| Properties | Measuring method | Unit | Value |
| :---: | :---: | :---: | :---: |
| Density | ISO 1183 | $\mathrm{~kg} / \mathrm{m}^{3}$ | 905 |
| Melt Flow Rate $230^{\circ} \mathrm{C} / 2.16 \mathrm{~kg}$ | ISO 1133 | $\mathrm{~g} / 10 \mathrm{~min}$. | 0.3 |
| Modulus of Elasticity in Tension $(1 \mathrm{~mm} / \mathrm{min})$ | ISO 527 | MPa | 900 |
| Tensile Stress at Yield $(50 \mathrm{~mm} / \mathrm{min})$ | ISO 527 | MPa | 25 |
| Charpy Impact Strength, notched $\left(+23^{\circ} \mathrm{C}\right)$ | ISO 179 | $\mathrm{~kJ} / \mathrm{m}^{2}$ | 40 |
| Coefficient of linear expansion | DIN 53752 | $\mathrm{~mm} / \mathrm{mK}$ | 0.15 |
| Thermal conductivity | DIN 52612 | $\mathrm{~W} / \mathrm{mK}$ | mm |
| Pipe surface roughness K |  | $\mathrm{KJ} / \mathrm{kg} \mathrm{K}$ | 0.24 |
| Specific heat at $20^{\circ} \mathrm{C}$ | Calorimeter |  | 2.0 |

### 1.1.4 Fields of Application

For more than 30 years, polypropylene has been successfully used in supply lines of buildings in many countries worldwide. The combination of such excellent properties as chemical resistance, homogeneous connection, resistance to pressure and easy laying make it a reliable and lasting system suitable for various applications. In many countries it is gradually replacing such traditional materials as copper and galvanized steel.

## Properties of POLO-ECOSAN

- Enormous durability thanks to high-quality materials and processing
- Homogeneous connection guarantees high operational reliability.
- High demands for hygiene guarantee perfect water quality.
- Good thermal load capacity, therefore high operational reliability.
- High chemical resistance guarantees high durability.
- Minor flow noise makes living highly comfortable.
- High dimensional accuracy and low weight, therefore time- and cost-saving pipe laying.


### 1.1.5 Possible Uses

The POLO-ECOSAN installation system fulfils a variety of demands made on supply lines. It is suitable for universal use in:

- New buildings
- Refurbishment
- Repairs;
in drinking water installations for cold and hot water pipes in residential buildings, hospitals, hotels, office buildings, schools, etc., for example:
- Service connections
- Boiler connections
- Water distributing systems
- Rising lines
- Floor-level distribution
- Fittings
as well as piping networks for:
- Rainwater systems
- Outside pipe laying


## SYSTEM DESCRIPTION

- Compressed air systems
- Agriculture and horticulture
- Industries, for example the transportation of aggressive media (acids, alkaline solutions, etc.), taking into account its resistance to chemical agents
- Climate technology
- Chilled water technology
- Heating installations
- Shipbuilding
- Further media and possible applications upon request.

POLO-ECOSAN is not suitable for:

- Industrial gases
- Flammable liquids and gases
- Coolants/Refrigerants


### 1.2 POLO-ECOSAN Pipes

### 1.2.1 Overview

POLO-ECOSAN, the high-grade installation pipe made of polypropylene, POLO-ECOSAN ML5, POLO-ECOSAN ML3 and POLO-UV ML5, the multilayer fibre-reinforced composite pipes, guarantee reliable, durable and flawless supply in installation systems.

Wall thickness, pipe material and temperature range are the factors that decide the level of the resistance of a plastic pipe system to pressure.

POLOPLAST pipes are available in various wall thicknesses:

|  | Product range overview POLO-ECOSAN pipes |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diameter in mm | 20 | 25 | 32 | 40 | 50 | 63 | 75 | 90 | 110 | 125 | 160 | 200 | 250 |
| POLO-ECOSAN SDR 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| POLO-ECOSAN SDR 11 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| POLO-ECOSAN ML5 SDR 7.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| POLO-ECOSAN ML3 SDR 11 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| POLO-UV ML5 SDR 7.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |

Pipes 20-125 mm = socket welding
Pipes 160-250 mm = butt welding

POLO-ECOSAN

POLO-ECOSAN ML5

POLO-ECOSAN ML3


CALCULATED LIFETIME OF MORE THAN 50 YEARS

[^0]
## SYSTEM DESCRIPTION

## 1．2．2 POLO－ECOSAN

The traditional POLO－ECOSAN mono－pipe is made of PP－R．

## 1．2．2．1 Properties of the material

The physical and chemical properties have been chosen to meet the specific demands of drinking water systems．
Regular testing by in－house and external monitoring guarantee its suitability for various kinds of application．

## 1．2．2．2 Specification

Classification of operational conditions：application class according to EN ISO 15874
－SDR 6：class $1 / 10$ bar，class $2 / 8$ bar
－SDR 11：class 1／6 bar，class 2／4 bar

Info：Explanation on SDR and operational conditions see page 39／40．
Coefficient of linear expansion：$\alpha 0.15 \mathrm{~mm} / \mathrm{mK}$

## 1．2．2．3 Advantages

－Homogeneous connection
－Quick and easy assembly
－Resistance to corrosion
－Neutral in taste and odour
－Smooth pipe inner surface
－Good heat and sound insulation properties

### 1.2.3 POLO-ECOSAN ML5

The POLO-ECOSAN ML5 pipe represents a milestone in PP-R development. A 5-layer fibre pipe made of PP-R with glass fibre and the PP-RCT material.

### 1.2.3.1 Properties of the material

PP-RCT: Polypropylene random copolymer with modified crystalline structure and increased resistance at elevated temperature. This material represents a new generation of the tried and tested PP-R material. Especially with higher temperatures, the increased crystallinity of PP-RCT provides an improved creep-depending-on-time behaviour under internal compression.
PP = polypropylene
$R=$ random
C = crystallinity
T = temperature

This is why pipes made from this material can have thinner walls and consequently larger inner diameters. Designers and plumbers are offered convincing advantages from this circumstance. Thanks to the larger inner diameter, the hydraulic capacity of the pipes increases, which is specifically advantageous in systems that need to transport large amounts of water, for example in high-rise buildings.

Pipes made of PP-RCT are accepted according to the EN ISO 15874 standard and the EN ISO 21003 standard on multilayer pipes, and represent the state of the art. The same well-tried connection technique is used for pipes and fittings made of PP-RCT as for PP-R pipes.

### 1.2.3.2 Distribution of layers



## 1. Exterior PP-R layer

The exterior layer made of high-grade PP-R provides the colour code and guarantees flawless and reliable welding of pipe and fitting.

## 2. Second exterior layer made of HPCE, a special POLOPLAST compound material

This PP-R glass fibre compound material has been specially developed by POLOPLAST Polymer Engineering and represents the result of many years of research in this field. The perfect connection of glass fibre and PP-R provides excellent linear expansion, deformation properties, as well as good resistance to impact loads at low temperatures.

## 3. Central layer made of PP-RCT

PP-RCT is a polypropylene random copolymer with a modified crystalline structure. This material improves the long-term behaviour during longer operational periods, particularly, at increased temperatures.

## 4. Second inner layer made of HPCE, the special POLOPLAST compound material

This layer also provides excellent properties, such as linear expansion, deformation and good resistance to impact load at low temperatures.

## 5. Inner layer made of PP-RCT

In the same way as the central layer, this layer guarantees improved long-term behaviour during longer operational periods at increased temperatures. Smooth pipe inner surfaces prevent sediments and incrustations.

## SYSTEM DESCRIPTION

## 1．2．3．3 Specification

Material：PP－R／PP－GF／PP－RCT／PP－GF／PP－RCT

Pipe series：SDR 7.4 ／S 3.2 colour：green with silver stripe

Classification of operational conditions：application class according to EN ISO 15874
－SDR 7．4：class $1 / 8$ bar，class 2／8 bar

Info：Explanation on SDR and operational conditions see page 39／40．

Coefficient of linear expansion：$\alpha 0.038 \mathrm{~mm} / \mathrm{mK}$ ；tested and approved by a third party：OFI Institute，Vienna

## 1．2．3．4 Advantages

－Lower linear expansion reduced by $75 \%$ as compared to a PP－R standard pipe
－Improved resistance to internal pressure at increased temperatures as compared to a PP－R standard pipe，thanks to the PP－RCT material
－Increased stability allows longer distances between the fastening points
－Increased flow rate increased by approximately $16 \%$ thanks to thinner walls at unchanged dimension and pressure strain
－Higher resistance to impact loads－special compound materials increase the resistance to impact loads
－Good chemical resistance thanks to the PP－RCT material

## 1．2．3．5 Comparison of Linear Expansion

This comparison distinctly shows the linear expansion caused by temperature changes of a standard PP－R pipe and the POLO－ECOSAN ML5 pipe．
Linear expansion reduces by $75 \%$ ．


Comparison of linear expansion values

## 1. Exterior PP-R UV layer

The first layer provides UV protection and is made of specially stabilised PP-R to make the pipe highly reliable and resistant to ageing caused by UV radiation.

## 2. Second exterior layer made of HPCE, the special POLOPLAST compound material

This PP-R glass fibre compound material has been specially developed by POLOPLAST Polymer Engineering and represents the result of many years of research in this field. The perfect connection of glass fibre and PP-R provides excellent linear expansion, deformation properties, as well as good resistance to impact loads at low temperatures.

## 3. Central layer made of PP-RCT

PP-RCT is a polypropylene random copolymer with a modified crystalline structure. This new material improves the long-term behaviour during longer operational periods, particularly, at increased temperatures.

## 4. Second inner layer made of HPCE, a special POLOPLAST compound material

This layer also provides excellent properties, such as linear expansion, deformation and good resistance to impact load at low temperatures.

## 5. Inner layer made of PP-RCT

In the same way as for the central layer, we guarantee improved long-term behaviour of this layer during longer operational periods at increased temperatures. Smooth pipe inner surfaces prevent sediments and incrustations.

### 1.2.4.3 Processing

The pipes are installed using the existing fittings programme, without any additional operations. The POLO-UV ML5 pipe can be welded directly, with no need of peeling off the outer layer. Thus, pipes and fittings can be installed in the usual simple and safe way.

The fittings of the POLO-ECOSAN product line using the green colour are not long-term resistant to UV light. Suitable measures need to be taken separately to protect them.

## SYSTEM DESCRIPTION

## 1．2．4．4 Specification

Material：PP－R UV／PP－GF／PP－RCT／PP－GF／PP－RCT

Pipe series：SDR 7.4 ／S 3.2 colour：black

Classification of operational conditions：application class according to EN ISO 15874
－SDR 7．4：class 1／8 bar，class 2／6 bar

Info：Explanation on SDR and operational conditions see page 39／40．

Coefficient of linear expansion：$\alpha 0.038 \mathrm{~mm} / \mathrm{mK}$ ； tested and approved by the external OFI Institute，Vienna

## 1．2．4．5 Advantages

－ 10 years of warranty on resistance to UV radiation has been tested by a third party
－No additional operations required－usual and safe homogeneous welding of pipe and moulded part
－Low linear expansion－reduced by $75 \%$ as compared to a PP－R standard pipe
－Increased stability allows longer distances between the fastening points
－Increased flow rate－increased by approximately $16 \%$ thanks to thinner walls at unchanged dimension and pressure strain
－Higher resistance to impact loads－special compound materials increase the resistance to impact loads

## 1．2．4．6 Examined Resistance to UV Radiation

The resistance of the POLO－UV ML5 pipe to UV radiation has been tested by an acknowledged testing la－ boratory．During the entire test period samples were taken at certain intervals，which were then subjected to strength tests to examine them for possible changes of the material＇s mechanical properties．At the same time， material stability tests were carried out on a regular basis．The radiation intensity used for these tests was the same as in Aswan／Egypt over a period of more than 10 years．

## SYSTEM DESCRIPTION

### 1.2.5 POLO-ECOSAN ML3

The POLO-ECOSAN ML3 fibre compound pipe represents an addition to the comprehensive product line with larger dimensions starting from 125 mm and using the tried and tested 3-layer technology.
1.2.5.1 Distribution of layers


## 1. External layer made of PP-R-CT

The outer layer made of high-grade polypropylene granulate protects the pipe from surface damage resulting from mechanical external forces.

## 2. Intermediate layer made of PP-RCT-glass fibre compound

The fibre reinforcement in the intermediate layer increases the stability and, in combination with the other two layers, provides low deflection, reduced linear expansion, a high load carrying capacity, increased robustness and resistance to pressure.

## 3. Internal layer made of PP-RCT

Used as material for the internal layer, high-grade polypropylene granulate not only provides for high temperature resistance, but also ensures the pipe's resistance to corrosion, pitting, leaching and mechanical abrasion.

### 1.2.5.2 Specification

Material: PP-RCT / PP-RCT GF / PP-RCT

Pipe series: SDR 11 / S 5 colour: green

Classification of Operational Conditions: application class according to EN ISO 15874

- SDR 11: class $1 / 6$ bar, class 2/6 bar

Info: Explanation on SDR and operational conditions see page 39/40.

Coefficient of linear expansion: $\alpha 0.05 \mathrm{~mm} / \mathrm{mK}$

### 1.2.5.3 Advantages

- Low linear expansion
- Optimal stability
- Minor sagging
- Good chemical resistance thanks to the PP-RCT material
- Improved resistance to internal pressure at increased temperatures as compared to a PP-R standard pipe, thanks to the PP-RCT material


## SYSTEM DESCRIPTION

## 1．2．6 Pipe Labelling

The pipes must be durably labelled in the following way： Example：

| Outer diameter $x$ wall thickness | $25 \times 4.2$ |
| :--- | :--- |
| Product name | POLO－ECOSAN |
| Designation of material | PP－R |
| SDR wall thickness ratio | SDR 6 |
| Pipe series S | S 2.5 |
| Dimensional class according to EN ISO 15874 | A |
| Class of application and admissible operational pressure according to EN ISO 15874 | Class 1／10 bar，Class 2／8 bar |
| Range of use | 20 bar／20C，10 bar／70C |
| Suitability for drinking water | TW |
| Impermeability to light | opaque |
| Product standards | DIN 8077／8078，EN ISO 15874 |
| Certificates，approvals | SKZ A 553 |
| Material labelling | Material |
| Machine number | Machine |
| Date of manufacture | DAY MONTH YEAR HOUR：MINUTE |
| Manufacturer | POLOPLAST |
|  |  |

## $25 \times 4.2$ POLO－ECOSAN MADE IN GERMANY

mprint and order：

PP－R SDR 6／S 2．5 A Class 1／10 bar Class 2／8 bar 20 bar／20C 10 bar／70C TW opaque DIN 8077／78 EN ISO 15874 SKZ A 553 Material Machine Day Month Year Hour：Minute

### 1.3 Product Line

### 1.3.1 POLO-ECOSAN Pipes

POLO-ECOSAN Pipe SDR 6 / S 2.5
PP-R for hot and cold water acc. to DIN 8077/78 and EN ISO 15874, class 1/10 bar, class $2 / 8$ bar, SKZ certificate A 553, colour green with red line


| Item <br> No. | Outer <br> $\emptyset \mathbf{~ m m}$ | Wall thick- <br> ness $\mathbf{~ m m}$ | Inner $\emptyset$ <br> $\mathbf{m m}$ | DN | Water <br> Content I/m | Weight <br> $\mathbf{k g / m}$ | Packing unit <br> parcel/bar |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 6 0 0 2}$ | 20 | 3.4 | 13.2 | 12 | 0.137 | 0.172 | $100 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16003 | 25 | 4.2 | 16.6 | 15 | 0.216 | 0.266 | $60 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16004 | 32 | 5.4 | 21.2 | 20 | 0.353 | 0.434 | $40 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16005 | 40 | 6.7 | 26.6 | 25 | 0.556 | 0.671 | $20 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16006 | 50 | 8.3 | 33.4 | 32 | 0.866 | 1.040 | $20 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16007 | 63 | 10.5 | 42.0 | 40 | 1.385 | 1.650 | $12 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16008 | 75 | 12.5 | 50.0 | 50 | 1.936 | 2.340 | $8 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16009 | 90 | 15.0 | 60.0 | - | 2.827 | 3.360 | $4 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16010 | 110 | 18.3 | 73.4 | 65 | 4.208 | 5.010 | $4 \mathrm{~m} / 4 \mathrm{~m}$ | S |

POLO-ECOSAN Pipe SDR 11 / S 5
PP-R for hot and cold water acc. to DIN 8077/78 and EN ISO 15874, class 1/6 bar, class 2/4 bar, colour green with blue line


| Item <br> No. | Outer <br> $\emptyset \mathbf{~ m m}$ | Wall thick- <br> ness $\mathbf{~ m m}$ | Inner $\emptyset$ <br> $\mathbf{m m}$ | DN | Water <br> Content I/m | Weight <br> $\mathbf{k g} / \mathbf{m}$ | Packing unit <br> parcel/bar |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 6 1 0 2}$ | 20 | 1.9 | 16.2 | 15 | 0.206 | 0.107 | $100 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16103 | 25 | 2.3 | 20.4 | 20 | 0.327 | 0.164 | $60 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16104 | 32 | 2.9 | 26.2 | 25 | 0.531 | 0.261 | $40 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16105 | 40 | 3.7 | 32.6 | 32 | 0.834 | 0.412 | $20 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16106 | 50 | 4.6 | 40.8 | 40 | 1.307 | 0.638 | $20 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16107 | 63 | 5.8 | 51.4 | 50 | 2.075 | 1.010 | $12 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16108 | 75 | 6.8 | 61.4 | - | 2.941 | 1.410 | $8 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16109 | 90 | 8.2 | 73.6 | 65 | 4.254 | 2.030 | $4 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16110 | 110 | 10.0 | 90.0 | 80 | 6.362 | 3.010 | $4 \mathrm{~m} / 4 \mathrm{~m}$ | S |

POLO-ECOSAN ML5 Fibre Pipe SDR 7.4 / S 3.2 PP-R, PP-RCT for hot and cold water acc. to DIN 8077/78 and EN ISO 15874, class $1 / 8$ bar, class $2 / 8$ bar, SKZ certificate A 634, colour green with silver line


| Item <br> No. | Outer <br> $\emptyset \mathbf{~ m m}$ | Wall thick- <br> ness $\mathbf{~ m m}$ | Inner $\boldsymbol{\emptyset}$ <br> $\mathbf{m m}$ | $\mathbf{D N}$ | Water <br> Content $\mathbf{l / m}$ | Weight <br> $\mathbf{k g} / \mathbf{m}$ | Packing unit <br> parcel/bar |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16322 | 20 | 2.8 | 14.4 | 15 | 0.163 | 0.149 | $100 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16323 | 25 | 3.5 | 18.0 | 20 | 0.254 | 0.236 | $60 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16324 | 32 | 4.4 | 23.2 | 25 | 0.423 | 0.385 | $40 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16325 | 40 | 5.5 | 29.0 | 32 | 0.661 | 0.584 | $20 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16326 | 50 | 6.9 | 36.2 | 40 | 1.029 | 0.916 | $20 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16327 | 63 | 8.6 | 45.8 | 50 | 1.647 | 1.474 | $12 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16328 | 75 | 10.3 | 54.4 | - | 2.324 | 2.048 | $8 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16329 | 90 | 12.3 | 65.4 | 65 | 3.359 | 2.922 | $4 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 16330 | 110 | 15.1 | 79.8 | 80 | 5.001 | 4.374 | $4 \mathrm{~m} / 4 \mathrm{~m}$ | S |

POLO-ECOSAN ML3 Fibre Pipe SDR 11 / S 5 PP-RCT for hot and cold water acc. to DIN 8077/78 and EN ISO 15874, class 1/6 bar, class 2/6 bar, colour green with silver line


| Item <br> No. | Outer <br> $\emptyset \mathbf{m m}$ | Wall thick- <br> ness $\mathbf{~ m m}$ | Inner Ø <br> $\mathbf{m m}$ | DN | Water <br> Content $\mathbf{I / m}$ | Weight <br> $\mathbf{k g} / \mathbf{m}$ | Packing unit <br> parcel/bar |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16332 | 125 | 11.4 | 102.2 | 100 | 8.200 | 4.065 | $4 \mathrm{~m} / 4 \mathrm{~m}$ | MQ |
| 16333 | $160^{\star}$ | 14.6 | 130.8 | 125 | 13.440 | 6.645 | $4 \mathrm{~m} / 4 \mathrm{~m}$ | MQ |
| 16334 | $200^{\star}$ | 18.2 | 163.6 | 150 | 21.031 | 10.230 | $4 \mathrm{~m} / 4 \mathrm{~m}$ | MQ |
| 16335 | $250^{\star}$ | 22.7 | 204.6 | 200 | 32.865 | 16.125 | $4 \mathrm{~m} / 4 \mathrm{~m}$ | MQ |

## SYSTEM DESCRIPTION

POLO－UV ML5 Fibre Pipe with UV protection layer，SDR 7.4 ／S 3.2 ／ PP－R／PP－RCT for hot and cold water acc．to DIN 8077／78 and EN ISO 15874， class 1／8 bar，class 2／6 bar， colour black


| Item <br> No． | Outer <br> $\boldsymbol{\emptyset} \mathbf{~ m m}$ | Wall thick－ <br> ness $\mathbf{~ m m}$ | Inner $\boldsymbol{\emptyset}$ <br> $\mathbf{m m}$ | DN | Water <br> Content $\mathbf{l / m}$ | Weight <br> $\mathbf{k g} / \mathbf{m}$ | Packing unit <br> parcel／bar |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 40322 | 20 | 2.8 | 14.4 | 15 | 0.163 | 0.149 | $100 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 40323 | 25 | 3.5 | 18.0 | 20 | 0.254 | 0.236 | $60 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 40324 | 32 | 4.4 | 23.2 | 25 | 0.423 | 0.385 | $40 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 40325 | 40 | 5.5 | 29.0 | 32 | 0.661 | 0.584 | $20 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 40326 | 50 | 6.9 | 36.2 | 40 | 1.029 | 0.916 | $20 \mathrm{~m} / 4 \mathrm{~m}$ | S |
| 40327 | 63 | 8.6 | 45.8 | 50 | 1.647 | 1.474 | $12 \mathrm{~m} / 4 \mathrm{~m}$ | S |

## Support for pipes，galvanized

（for horizontally installed pipes，
self－clamping up to $\varnothing 75 \mathrm{~mm}$ ）

| Item No． | Diameter <br> in $\mathbf{m m}$ | Packing unit <br> parcel／bar |
| :---: | :---: | :---: |
| 14902 | 20 | $75 / 3 \mathrm{~m}$ |
| 14903 | 25 | $75 / 3 \mathrm{~m}$ |
| 14904 | 32 | $75 / 3 \mathrm{~m}$ |
| 14905 | 40 | $15 / 3 \mathrm{~m}$ |
| 14906 | 50 | $15 / 3 \mathrm{~m}$ |
| 14907 | 63 | $15 / 3 \mathrm{~m}$ |
| 14908 | 75 | $15 / 3 \mathrm{~m}$ |
| 14909 | 90 | $15 / 3 \mathrm{~m}$ |
| 14910 | 110 | $15 / 3 \mathrm{~m}$ |

## 1．3．2 POLO－ECOSAN Fittings

| POLO－ECOSAN Long cross－over section | Item No． | Diameter in mm | Packing unit <br> carton／bag |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 16502 | 20 | $150 / 10$ | S |
|  | 16503 | 25 | $100 / 10$ | S |
|  | 16504 | 32 | $70 / 10$ | S |
|  | 16506 | 40 | $25 / 5$ | MQ |

## SYSTEM DESCRIPTION

| QUALITY MANAGEMENT | INITIAL OPERATION | ASSEMBLY GUIDELINES | WELDING TECHNOLOGY | PLANNING AND DESIGN | SYSTEM REQUIREMENTS | DRINKING WATER HYGIENE | TRANSPORTATION AND STORAGE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| POLO-ECOSAN Welding socket | Item No. | Diameter in mm | Packing unit carton/bag |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 17002 | 20 | $600 / 10$ | S |
|  | 17003 | 25 | 400 / 10 | S |
|  | 17004 | 32 | 250/10 | S |
|  | 17005 | 40 | 170/10 | S |
|  | 17006 | 50 | $100 / 5$ | S |
|  | 17007 | 63 | $50 / 1$ | S |
|  | 17008 | 75 | $40 / 1$ | S |
|  | 17009 | 90 | $24 / 1$ | S |
|  | 17010 | 110 | 15/1 | S |
|  | 17011 | 125 | 12/1 | MQ |

## POLO-ECOSAN Reducer male / female



| Item No. | Diameter in mm | Packing unit carton/bag |  |
| :---: | :---: | :---: | :---: |
| 17603 | 25/20 | $300 / 10$ | S |
| 17605 | $32 / 20$ | 250/10 | S |
| 17606 | 32/25 | 200/10 | S |
| 17608 | 40 / 20 | $400 / 5$ | S |
| 17609 | $40 / 25$ | $300 / 5$ | S |
| 17610 | 40 / 32 | 200/5 | S |
| 17612 | $50 / 20$ | $250 / 5$ | S |
| 17613 | $50 / 25$ | 150/5 | S |
| 17614 | $50 / 32$ | $200 / 5$ | S |
| 17615 | 50/40 | $150 / 5$ | S |
| 17618 | $63 / 25$ | 100/1 | S |
| 17619 | $63 / 32$ | 120 / 1 | S |
| 17620 | $63 / 40$ | 100/1 | S |
| 17621 | 63/50 | 75/1 | S |
| 17627 | 75/50 | $50 / 1$ | S |
| 17628 | 75/63 | $50 / 1$ | S |
| 17634 | 90/50 | $40 / 1$ | S |
| 17635 | 90/63 | $40 / 1$ | S |
| 17636 | 90/75 | $30 / 1$ | S |
| 17643 | $110 / 63$ | $30 / 1$ | S |
| 17644 | 110 / 75 | 25/1 | S |
| 17645 | 110/90 | 20/1 | S |
| 17646 | 125/110 | 15/1 | MQ |

## SYSTEM DESCRIPTION

| POLO-ECOSAN Welding elbow $90{ }^{\circ}$ | Item No. | Diameter in mm | Packing unit carton/bag |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 17042 | 20 | 500 / 10 | S |
|  | 17043 | 25 | 300 / 10 | S |
|  | 17044 | 32 | 150/10 | S |
|  | 17045 | 40 | 100/5 | S |
|  | 17046 | 50 | $50 / 5$ | S |
|  | 17047 | 63 | $25 / 1$ | S |
|  | 17048 | 75 | 15/1 | S |
|  | 17049 | 90 | 12 / 1 | S |
|  | 17050 | 110 | $12 / 1$ | S |
|  | 17051 | 125 | 8/1 | MQ |
| POLO-ECOSAN Butt welding elbow $90^{\circ}$ | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  | 17053 / 2 | 160 | 1/1 | MQ |
|  | 17055 / 2 | 200 | 1/1 | MQ |
|  | 17057 / 2 | 250 | 1/1 | MQ |
| POLO-ECOSAN Welding elbow male / female | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  | 17062 | 20 | 250 / 10 | S |
|  | 17063 | 25 | 150 / 10 | S |
|  | 17064 | 32 | $80 / 10$ | S |
|  | 17065 | 40 | $40 / 5$ | S |
| POLO-ECOSAN Welding elbow $45^{\circ}$ | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  | 17102 | 20 | 200 / 10 | S |
|  | 17103 | 25 | 150 / 10 | S |
|  | 17104 | 32 | 100 / 10 | S |
|  | 17105 | 40 | $50 / 5$ | S |
|  | 17106 | 50 | $25 / 5$ | S |
|  | 17107 | 63 | 12/1 | S |
|  | 17108 | 75 | $20 / 1$ | S |
|  | 17109 | 90 | 15/1 | S |
|  | 17110 | 110 | 8/1 | S |
|  | 17111 | 125 | $5 / 1$ | MQ |
| POLO-ECOSAN Butt welding elbow $45^{\circ}$ | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  | 17113 / 2 | 160 | 1/1 | MQ |
|  | 17115 / 2 | 200 | 1/1 | MQ |
|  | 17117 / 2 | 250 | 1/1 | MQ |

## SYSTEM DESCRIPTION

| POLO-ECOSAN Butt welding elbow $\mathbf{4 5}^{\circ}$ male / <br> female | Item No. | Diameter in mm | Packing unit <br> carton/bag |  |
| :--- | :---: | :---: | :---: | :---: |
|  | 17122 | 20 | $300 / 10$ | S |
|  | 17123 | 25 | $200 / 10$ | S |
|  | 17124 | 32 | $80 / 10$ | S |
|  | 17125 | 40 | $60 / 5$ | S |

POLO-ECOSAN Butt welding tee


| Item No. | Diameter in mm | Packing unit <br> carton/bag |  |
| :---: | :---: | :---: | :---: |
| $17213 / 2$ | 160 | $1 / 1$ | MQ |
| $17215 / 2$ | 200 | $1 / 1$ | MQ |
| $17217 / 2$ | 250 | $1 / 1$ | MQ |

Reduced tee on request


| Item No． | Diameter in mm | Packing unit carton／bag |  |
| :---: | :---: | :---: | :---: |
| 17250 | $25 \times 20 \times 20$ | 250 ／ 10 | S |
| 17251 | $20 \times 25 \times 20$ | 250 ／ 10 | MQ |
| 17254 | $25 \times 20 \times 25$ | 250 ／ 10 | S |
| 17256 | $25 \times 25 \times 20$ | 250 ／ 10 | MQ |
| 17261 | $32 \times 20 \times 20$ | 120／5 | MQ |
| 17266 | $32 \times 25 \times 20$ | 120 ／ 5 | MQ |
| 17267 | $32 \times 20 \times 25$ | 120／5 | MQ |
| 17269 | $32 \times 25 \times 25$ | 120 ／ 5 | MQ |
| 17273 | $32 \times 20 \times 32$ | $120 / 5$ | S |
| 17275 | $32 \times 25 \times 32$ | $120 / 5$ | S |
| 17301 | $40 \times 32 \times 32$ | $80 / 5$ | MQ |
| 17305 | $40 \times 20 \times 40$ | $80 / 5$ | S |
| 17307 | $40 \times 25 \times 40$ | $80 / 5$ | S |
| 17309 | $40 \times 32 \times 40$ | $80 / 5$ | S |
| 17311 | $50 \times 20 \times 50$ | 40 ／ 2 | MQ |
| 17334 | $50 \times 25 \times 50$ | $40 / 2$ | S |
| 17336 | $50 \times 32 \times 50$ | 40 ／ 2 | S |
| 17338 | $50 \times 40 \times 50$ | 40 ／ 2 | S |
| 17340 | $63 \times 20 \times 63$ | $25 / 1$ | S |
| 17352 | $63 \times 25 \times 63$ | 25／1 | S |
| 17354 | $63 \times 32 \times 63$ | 25／1 | S |
| 17356 | $63 \times 40 \times 63$ | 25／1 | S |
| 17358 | $63 \times 50 \times 63$ | 25／1 | S |
| 17360 | $75 \times 20 \times 75$ | 15／1 | MQ |
| 17370 | $75 \times 25 \times 75$ | 15／1 | S |
| 17372 | $75 \times 32 \times 75$ | 15／1 | S |
| 17374 | $75 \times 40 \times 75$ | 15／1 | S |
| 17376 | $75 \times 50 \times 75$ | 15／1 | S |
| 17378 | $75 \times 63 \times 75$ | 15／1 | S |
| 17394 | $90 \times 50 \times 90$ | 12／1 | MQ |
| 17396 | $90 \times 63 \times 90$ | 12／1 | S |
| 17398 | $90 \times 75 \times 90$ | 8／1 | S |
| 17414 | $110 \times 63 \times 110$ | 14／1 | S |
| 17416 | $110 \times 75 \times 110$ | $6 / 1$ | S |
| 17418 | $110 \times 90 \times 110$ | $6 / 1$ | S |
| 17420 | $125 \times 110 \times 125$ | $6 / 1$ | MQ |


|  | POLO-ECOSAN Weld-in saddle with welding sleeve | Item No. | Diameter in mm | Packing unit carton/bag |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 17741 | $40 / 20$ | $250 / 5$ | S |
|  |  | 17742 | $40 / 25$ | $250 / 5$ | S |
|  |  | 17744 | $50 / 20$ | $250 / 5$ | S |
|  |  | 17745 | $50 / 25$ | $250 / 5$ | S |
|  |  | 17747 | $63 / 20$ | $200 / 5$ | S |
|  |  | 17748 | $63 / 25$ | $200 / 5$ | S |
|  |  | 17749 | $63 / 32$ | $150 / 5$ | S |
|  |  | 17750 | $75 / 20$ | $200 / 5$ | S |
|  |  | 17751 | $75 / 25$ | $200 / 5$ | S |
|  |  | 17752 | $75 / 32$ | 120 / 5 | S |
|  |  | 17754 | $90 / 20$ | $200 / 5$ | S |
|  |  | 17756 | $90 / 25$ | $200 / 5$ | S |
|  |  | 17758 | 90/32 | $150 / 5$ | S |
|  |  | 17760 | 110 / 20 | $200 / 5$ | S |
|  |  | 17761 | 110/25 | $150 / 5$ | S |
|  |  | 17762 | 110/32 | $120 / 5$ | S |
|  |  | 17765 | 125 / 20 | $200 / 5$ | S |
|  |  | 17766 | 125 / 25 | $150 / 5$ | S |
|  |  | 17767 | 125 / 32 | 100/5 | S |
|  |  | 17770 | 160 / 20 | $200 / 5$ | MQ |
|  |  | 17771 | 160 / 25 | $200 / 5$ | MQ |
|  |  | 17772 | 160 / 32 | $100 / 5$ | MQ |
|  | POLO-ECOSAN Weld-in saddle with an internal screw thread for wrench - female | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 18352 | $40 \times 1 / 2^{\prime \prime}$ | 100/5 | S |
|  |  | 18353 | $40 \times 3 / 4{ }^{\prime \prime}$ | $100 / 5$ | S |
|  |  | 18354 | $50 \times 1 / 2^{\prime \prime}$ | $100 / 5$ | S |
|  |  | 18355 | $50 \times 3 / 4{ }^{\prime \prime}$ | $100 / 5$ | S |
|  |  | 18356 | $63 \times 1 / 2^{\prime \prime}$ | $100 / 5$ | S |
|  |  | 18357 | $63 \times 3 / 4{ }^{\prime \prime}$ | $50 / 5$ | S |
|  |  | 18358 | $63 \times 1$ " | $50 / 5$ | S |
|  |  | 18359 | $75 \times 1 / 2^{\prime \prime}$ | $80 / 5$ | S |
|  |  | 18360 | $75 \times 3 / 4 "$ | $80 / 5$ | S |
|  |  | 18361 | $75 \times 1$ " | $50 / 5$ | S |
|  |  | 18362 | $90 \times 1 / 2^{\prime \prime}$ | $80 / 5$ | S |
|  |  | 18363 | $90 \times 3 / 4 "$ | $80 / 5$ | S |
|  |  | 18364 | $90 \times 1$ " | $50 / 5$ | S |
|  |  | 18366 | $110 \times 1 / 2^{\prime \prime}$ | $100 / 5$ | S |
|  |  | 18367 | $110 \times 3 / 4$ " | $80 / 5$ | S |
|  |  | 18368 | $110 \times 1$ " | $50 / 5$ | S |
|  |  | 18370 | $125 \times 1 / 2^{\prime \prime}$ | $50 / 5$ | S |
|  |  | 18371 | $125 \times 3 / 4 "$ | $50 / 5$ | S |
|  |  | 18372 | $125 \times 1$ " | $50 / 5$ | S |
|  |  | 18375 | $160 \times 1 / 2^{\prime \prime}$ | $100 / 5$ | MQ |
|  |  | 18376 | $160 \times 3 / 4 "$ | $50 / 5$ | MQ |
|  |  | 18377 | $160 \times 1$ " | $50 / 5$ | MQ |

Plastic drill see page 33, Welding tools see page 33

## SYSTEM DESCRIPTION

| POLO-ECOSAN End cap | Item No. | Diameter in mm | Packing unit carton/bag |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 17702 | 20 | 400 / 10 | S |
|  | 17703 | 25 | 250 / 10 | S |
|  | 17704 | 32 | 150 / 10 | S |
|  | 17705 | 40 | $100 / 5$ | S |
|  | 17706 | 50 | 60 / 5 | S |
|  | 17707 | 63 | $30 / 1$ | S |
|  | 17708 | 75 | $20 / 1$ | S |
|  | 17709 | 90 | $30 / 1$ | S |
|  | 17710 | 110 | 15/1 | S |
|  | 17711 | 125 | 12 / 1 | MQ |
|  |  |  |  |  |
| POLO-ECOSAN End cap | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  | 17712 / 2 | 160 | 1 | MQ |
|  | 17713/2 | 200 | 1 | MQ |
|  | 17714 / 2 | 250 | 1 | MQ |
|  |  |  |  |  |
| POLO-ECOSAN Flange bushing with gasket | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  | 17807 | 63 | $30 / 1$ | MQ |
|  | 17808 | 75 | $20 / 1$ | S |
|  | 17809 | 90 | 15/1 | S |
|  | 17810 | 110 | 12/1 | S |
|  | 17811 | 125 | 10/1 | S |
|  |  |  |  |  |
| POLO-ECOSAN Flange bushing with gasketPP-RCT, SDR 11 | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  | 17812 / 2 | 160 | 1 | S |
|  | 17814 / 2 | 200 | 1 | S |
|  | 17816 / 2 | 250 | 1 | S |

POLO-ECOSAN PP-flange, glass fibre reinforced, for flange bushing PN 16


| Item No. | Diameter in mm | DN | Packing unit <br> carton/bag |  |
| :---: | :---: | :---: | :---: | :---: |
| 14207 | 63 | 50 | 1 | S |
| 14208 | 75 | 65 | 1 | S |
| 14209 | 90 | 80 | 1 | S |
| 14210 | 110 | 100 | 1 | S |
| 14211 | 125 | 100 | 1 | S |
| 14212 | 160 | 150 | 1 | S |
| 14214 | 200 | 200 | 1 | S |
| 14216 | 250 | 250 | 1 | S |

## SYSTEM DESCRIPTION

|  | POLO-ECOSAN Socket for electric welding |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |



## SYSTEM DESCRIPTION

|  | POLO-ECOSAN Screw adapter, male, thread/pipe end | Item No. | Diameter in mm | Packing unit carton/bag |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 24172 | $20 \times 1 / 2^{\prime \prime}$ | 80/1 | MQ |
|  |  | 24173 | $25 \times 3 / 4{ }^{\prime \prime}$ | $50 / 1$ | S |
|  |  | 24174 | $32 \times 1$ " | $50 / 1$ | MQ |
|  |  | 24175 | $40 \times 11 / 4 "$ | 25/1 | MQ |
|  |  | 24176 | $50 \times 11 / 2^{\prime \prime}$ | $20 / 1$ | MQ |
|  |  | 24177 | $63 \times 2$ " | 15/1 | MQ |
|  | POLO-ECOSAN Screw adapter, female, thread/pipe end | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 24162 | $20 \times 1 / 2^{\prime \prime}$ | 80/1 | MQ |
|  | 4 | 24163 | $25 \times 3 / 4{ }^{\prime \prime}$ | $50 / 1$ | MQ |
|  |  | 24164 | $32 \times 1$ " | $50 / 1$ | MQ |
|  |  | 24165 | $40 \times 11 / 4{ }^{\prime \prime}$ | 25/1 | MQ |
|  |  | 24166 | $50 \times 11 / 2^{\prime \prime}$ | 20/1 | MQ |
|  |  | 24167 | $63 \times 2$ " | 15/1 | MQ |
|  | POLO-ECOSAN Screwed union plastic/brass $F$ with socket end | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 20043 | $20 \times 1 / 2^{\prime \prime}$ | 100/1 | S |
|  |  | 20045 | $20 \times 3 / 4 "$ | 100/1 | S |
|  |  | 20047 | $25 \times 3 / 4 "$ | 100/1 | S |
|  |  | 20048 | $25 \times 1$ " | 70/1 | S |
|  |  | 20050 | $32 \times 1{ }^{\prime \prime}$ | 70/1 | S |
|  |  | 20053 | $40 \times 11 / 4{ }^{\prime \prime}$ | $50 / 1$ | S |
|  |  | 20056 | $50 \times 11 / 2^{\prime \prime}$ | $30 / 1$ | S |
|  |  | 20058 | $63 \times 2$ " | 20/1 | S |
|  | POLO-ECOSAN Screwed union plastic/brass F with pipe end | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 20078 | $25 \times 1$ " | 70/1 | S |
|  |  | 20081 | $32 \times 11 / 4{ }^{\prime \prime}$ | $50 / 1$ | S |
|  |  | 20084 | $40 \times 11 / 2^{\prime \prime}$ | 50/1 | MQ |
|  | Reducing nipple, male | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 14102 | $3 / 4$ " $\times 1 / 2^{\prime \prime}$ | $260 / 1$ | S |
|  |  | 14104 | 1" $\times 3 / 4$ " | 200/1 | S |
|  |  | 14106 | $11 / 4$ " $\times 1$ " | 140/1 | S |
|  | Reducer male x female | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 14122 | $3 / 4$ " $\times 1 / 2^{\prime \prime}$ | $350 / 1$ | S |
|  |  | 14124 | 1"x $\times 1 / 4$ " | 240/1 | S |
|  |  | 14126 | $11 / 4^{\prime \prime} \times 1$ " | 180/1 | S |

## SYSTEM DESCRIPTION

## 1．3．4 POLO－ECOSAN Fittings and Accessories

| POLO－ECOSAN Wall union，female | Item No． | Diameter in mm | Packing unit carton／bag |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 18004 | $20 \times 1 / 2^{\prime \prime}$ | 100 ／ 10 | S |
|  | 18006 | $25 \times 1 / 2^{\prime \prime}$ | $80 / 10$ | S |
|  | 18007 | $25 \times 3 / 4{ }^{\prime \prime}$ | $80 / 10$ | S |

POLO－ECOSAN Double wall union，female， two outlets


| Item No． | Diameter in mm | Packing unit <br> carton／bag |  |
| :---: | :---: | :---: | :---: |
| 18016 | $25 \times 1 / 2^{\prime \prime}$ | $80 / 10$ | S |

Assembly plate，plastic，with screws for wall union， selectable distances
115 ／ 140 ／ $150 / 160 / 180$ mm

| Item No． | Diameter in mm | Packing unit <br> carton／bag |  |
| :---: | :---: | :---: | :---: |
| 15484 | $250 \times 45$ | $50 / 1$ | S |



| Item No． | Diameter in mm | Packing unit <br> carton／bag |  |
| :---: | :---: | :---: | :---: |
| 18024 | $20 \times 1 / 2^{\prime \prime}$ | $70 / 10$ | S |
| 18026 | $25 \times 1 / 2^{\prime \prime}$ | $50 / 10$ | S |

## SYSTEM DESCRIPTION

Assembly unit, galvanized, for wall union, with screws
Distance 150 / 80 mm

| Item No. | Diameter in mm | Packing unit <br> carton/bag |  |
| :---: | :---: | :---: | :---: |
| 15482 | $420 \times 60 \times 45$ | 1 | S |


| Assembly plug | Item No. | Diameter in mm | Packing unit <br> carton/bag |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | red $=15413$ <br> blue $=15414$ | 15413 | $1 / 2^{\prime \prime}$ | $200 / 10$ | S |
|  | 15414 | $1 / 2^{\prime \prime}$ | $200 / 10$ | S |  |

Assembly help with 2 plugs, distance 75 / 85 / 100 / 140 / 150 / 175

| Item No. | Diameter in $\mathbf{m m}$ | Packing unit <br> carton/bag |  |
| :---: | :---: | :---: | :---: |
| 15400 | $1 / 2^{\prime \prime}$ | $20 / 1$ | S |

## SYSTEM DESCRIPTION

### 1.3.5 POLO-ECOSAN Shutt-off devices and Accessories

POLO-ECOSAN Slanted seat valve, body without discharge screw

with discharge screw


| Item No. | Diameter in mm | Packing unit carton/bag |  |
| :---: | :---: | :---: | :---: |
| 20504 | $20 \times 3 / 4 "$ | 50 / 5 | S |
| 20505 | $25 \times 3 / 4 "$ | $50 / 5$ | S |
| 20508 | $32 \times 1$ " | $25 / 5$ | S |
| 20510 | $40 \times 11 / 4{ }^{\prime \prime}$ | 15/1 | S |
| 20512 | $50 \times 11 / 2^{\prime \prime}$ | 10/1 | MQ |
| 20534 | $20 \times 3 / 4{ }^{\prime \prime}$ | $40 / 5$ | S |
| 20535 | $25 \times 3 / 4 "$ | 40 / 5 | S |
| 20538 | $32 \times 1{ }^{\prime \prime}$ | $25 / 5$ | S |
| 20540 | $40 \times 11 / 4{ }^{\prime \prime}$ | $15 / 5$ | S |
| 20542 | $50 \times 11 / 2^{\prime \prime}$ | $8 / 1$ | MQ |


| Slanted seat valve, upper part | Item No. | Diameter in mm | Packing unit carton/bag |  |
| :---: | :---: | :---: | :---: | :---: |
| without backflow prevention and non-rising spindle | 14642 | 3/4" | 70/1 | S |
|  | 14643 | $1{ }^{\prime \prime}$ | $50 / 1$ | S |
|  | 14644 | 11/4" | $25 / 1$ | S |
|  | 14645 | 11/2" | $25 / 1$ | S |
| with backflow prevention and non rising spindle | 14662 | 3/4" | 25/1 | S |
|  | 14663 | $1{ }^{\prime \prime}$ | 40 / 1 | S |
|  | 14664 | 11/4" | $20 / 1$ | S |
|  | 14665 | 11/2" | $20 / 1$ | S |

POLO-ECOSAN Shut-off valve, body
without discharge screw


| Item No. | Diameter in mm | Packing unit <br> carton/bag |  |
| :---: | :---: | :---: | :---: |
| 20304 | $20 \times 3 / 4^{\prime \prime}$ | $50 / 5$ | S |
| 20306 | $25 \times 3 / 4$ " | $50 / 5$ | S |
| 20308 | $32 \times 1^{\prime \prime}$ | $30 / 5$ | S |
| 20310 | $40 \times 11 / 4^{\prime \prime}$ | $25 / 1$ | S |

with discharge screw


| 20324 | $20 \times 3 / 4^{\prime \prime}$ | $50 / 5$ | $M Q$ |
| :---: | :---: | :---: | :---: |
| 20326 | $25 \times 3 / 4^{\prime \prime}$ | $50 / 5$ | $M Q$ |
| 20328 | $32 \times 1$ " | $20 / 5$ | $M Q$ |
| 20330 | $40 \times 11 / 4^{\prime \prime}$ | $15 / 1$ | $M Q$ |

Shut-off valve, upper part


| Item No. | Diameter in mm | Packing unit <br> carton/bag |  |
| :---: | :---: | :---: | :---: |
| 14602 | $3 / 4$ " | $125 / 1$ | S |
| 14604 | $1^{\prime \prime}$ | $75 / 1$ | S |
| 14606 | $11 / 4^{\prime \prime}$ | $40 / 1$ | S |

## SYSTEM DESCRIPTION

|  | Concealed valve, upper part (in flexible length 60-110 mm) | Item No. | Diameter in mm | Packing unit carton/bag |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 14612 | 3/4" | 50 / 1 | S |
|  |  | 14614 | $1{ }^{\prime \prime}$ | 50 / 1 | S |
|  |  |  |  |  |  |
|  | Concealed valve, upper part | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 14611 | 3/4" | 40 / 1 | S |
|  |  | 14617 | $1{ }^{\prime \prime}$ | 40 / 1 | S |
|  | Concealed valve, upper part, public authority design | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 14622 | 3/4" | 60 / 1 | S |
|  |  | 14628 | 1 " | 40 / 1 | S |
|  | POLO-ECOSAN Ball valve <br> Handle: glass fibre reinforced polyamide, ball and stem: brass PTFE seats, NBR O-ring | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 20402 | 20 | 50 / 5 | S |
|  |  | 20403 | 25 | $25 / 5$ | S |
|  |  | 20404 | 32 | 15/1 | S |
|  |  | 20405 | 40 | 10/1 | S |
|  |  | 20412 | 50 | $6 / 1$ | S |
|  |  | 20414 | 63 | $5 / 1$ | S |
|  |  | 20416 | 75 | $5 / 1$ | MQ |
|  | POLO-ECOSAN Ball valve with chrome-plated upper part | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  | Handle: chrome-plated brass, ball and stem: brass PTFE | 20402 CR | 20 | $25 / 1$ | MQ |
|  |  | 20403 CR | 25 | 15/1 | MQ |
|  |  | 20404 CR | 32 | 10/1 | MQ |

## SYSTEM DESCRIPTION

### 1.3.6 POLO-ECOSAN Welding Machines, Tools and Accessories

Electronic welding device without attachments, 550 W up to $\varnothing 50 \mathrm{~mm}$

| Item No. | Diameter in mm | Packing unit <br> carton/bag |  |
| :---: | :---: | :---: | :---: |
| 15025 |  | 1 | S |



| Item No. | Diameter in mm | Packing unit <br> carton/bag |  |
| :---: | :---: | :---: | :---: |
| 15016 |  | 1 | S |

Electronic welding device, large version without attachments, 1400 W , up to $\varnothing 125 \mathrm{~mm}$

| Item No. | Diameter in mm | Packing unit <br> carton/bag |  |
| :---: | :---: | :---: | :---: |
| 15015 |  | 1 | S | 40 to 125 mm , complete with tools and welding



| Item No. | Diameter in mm | Packing unit <br> carton/bag |  |
| :---: | :---: | :---: | :---: |
| 15205 |  | 1 | S |


| Electronic butt welding machine from 160-250 mm | Item No. | Diameter in mm | Packing unit carton/bag |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 15207 |  | 1 | on request |
| Electronic welding machine for electric welding sockets, from 20-110 mm | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  | 15255 |  | 1 | S |
| Electronic welding machine for electric welding sockets up to 250 mm | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  | 15270 |  | 1 | on request |

## SYSTEM DESCRIPTION

|  | Welding case incl. device 550 W, bench-top device attachments Ø 20-63 mm | Item No. | Diameter in mm | Packing unit carton/bag |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 21310 |  | 1 | S |
|  |  |  |  |  |  |
|  | Welding case incl. device 1000 W , bench-top device, attachments $\varnothing 20-40 \mathrm{~mm}$, pipe cutter | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 15311 |  | 1 | S |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  | Ceiling welding machine from 63 to 125 mm | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 15210 |  | 1 | on request |
|  |  |  |  |  |  |
|  | Pipe cutter for pipes from $\varnothing 16$ to $\mathbf{4 0} \mathbf{~ m m}$ | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 15001 |  | 1 | S |
|  | Pipe cutter for pipes from $\varnothing 16$ to 63 mm | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 15003 |  | 1 | S |
|  |  |  |  |  |  |
|  | Pipe cutter for pipes from Ø $\mathbf{5 0}$ to 110 mm | Item No. | Diameter in mm | Packing unit carton/bag |  |
|  |  | 15007 |  | 1 | S |

## SYSTEM DESCRIPTION

| Welding attachment acc．to DVS－Guideline | Item No． | Diameter in mm | Packing unit carton／bag |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 15042 | 20 | 1 | S |
|  | 15043 | 25 | 1 | S |
|  | 15044 | 32 | 1 | S |
|  | 15045 | 40 | 1 | S |
|  | 15046 | 50 | 1 | S |
|  | 15047 | 63 | 1 | S |
|  | 15048 | 75 | 1 | S |
|  | 15049 | 90 | 1 | S |
|  | 15050 | 110 | 1 | S |
|  | 15051 | 125 | 1 | S |
| Saddle welding tools for weld－in saddles | Item No． | Diameter in mm | Packing unit carton／bag |  |
|  | 15065 | 40 （B25） | 1 | S |
|  | 15066 | 50 （B25） | 1 | S |
|  | 15067 | 63 （B25） | 1 | S |
|  | 15082 | 63 （B32） | 1 | S |
|  | 15068 | 75 （B25） | 1 | S |
|  | 15083 | 75 （B32） | 1 | S |
|  | 15069 | 90 （B25） | 1 | S |
| Extra order（B25）：Plastic Drill，item No．： 15095 <br> Extra order（B32）：Plastic Drill，item No．： 15096 | 15084 | 90 （B32） | 1 | S |
|  | 15070 | 110 （B25） | 1 | S |
|  | 15085 | 110 （B32） | 1 | S |
|  | 15071 | 125 （B25） | 1 | S |
|  | 15086 | 125 （B32） | 1 | S |
|  | 15087 | 160 （B25） | 1 | S |
|  | 15088 | 160 （B32） | 1 | S |
| Plastic Drill for weld－in saddles | Item No． | Diameter in mm | Packing unit carton／bag |  |
|  | 15095 | 25 （B25） | 1 | S |
|  | 15096 | 32 （B32） | 1 | S |

$\left.\begin{array}{|l|c|c|c|c|}\hline \text { Welding attachment for repair of holes up to } \varnothing 8 \mathrm{~mm} & \text { Item No．} & \text { Diameter in mm } & \begin{array}{c}\text { Packing unit } \\ \text { carton／bag }\end{array} & \\ \hline & & 15080 & & 1\end{array}\right]$ S

POLO－ECOSAN Welding plug for repair of holes up to Ø 8 mm

| Item No． | Diameter in mm | Packing unit <br> carton／bag |  |
| :---: | :---: | :---: | :---: |
| 21090 |  | $1200 / 100$ | S | S

## TRANSPORTATION AND STORAGE

### 2.1 Safety Instructions and Intended Use

- Carefully read the Technical Manual and the Operating Instructions before starting work.
- POLOPLAST Installation Systems may only be planned, assembled and started up as described in the present manual.
- For any deviating fields of application, make sure to obtain POLOPLAST‘S advice.
- All national and international safety regulations and regulations on accident prevention have to be observed.
- Planning, installation and start-up have to be carried out pursuant to the current directives, standards and regulations, as intended and in accordance with the state of the art.
- Only POLOPLAST system components are allowed to be used. The use of other components entails loss of guarantee (refer to the Letter of Guarantee on page 93).
- Observe the general safety regulations when handling assembly tools. Danger of burn.


## Handling Instructions

- POLOPLAST PP-R / PP-RCT pipes can generally be stored at any ambient temperature.
- Nevertheless, the material must never be subject to impacts or blows, particularly at temperatures below $5^{\circ} \mathrm{C}$.
- Do not drop the pipes when unloading them and protect them from falling objects.
- Select the place of storage so as to make sure that the pipes are always supported over their entire length.
- Before starting assembly, check the pipe and particularly the pipe ends for cracks or damage.
- Observe cleanliness when storing and laying the pipes and fittings. In order to protect the pipes and fittings against contamination, do not remove the packaging material before the material is used.
- Pipes (except UV pipes) and fittings must not be exposed to UV radiation over prolonged periods as this reduces the durability and the special properties of the pipes; provide protection of the pipes from the outside.
- At temperatures below zero, water supply pipes must be protected from frost, and drained, if necessary.
- Cut the pipes using only sharp tools.


Avoid sharp impacts and blows to the pipes, especially at low temperatures. Do not throw when unloading. Protect pipes from falling objects.


Do not use cracked or damaged pipes.


Do not expose pipes to UV-radiation for extended periods of time.


During polyfusion welding, do not twist the pipe or fitting; push the pipe and fitting joint together in a straight manner.


Protect pipes filled with water from freezing.


Put down pipes or pipe bundles carefully. Cover pipes in areas of falling rocks, etc.


Only cut pipes with sharp cutters.


Minor corrections can only be made during joining.


Drain lines in danger of freezing.

## DRINKING WATER HYGIENE

### 3.1 Drinking Water

Drinking water is our most important comestible, which is why water should always be available in optimum quality. The basic requirements on the quality of drinking water in Germany are defined in the "Drinking Water Ordinance (Trinkwasserverordnung)". To make sure to achieve the required quality parameters, the generally acknowledged codes of practice must also be observed. Drinking water hygiene has always been an important matter, particularly in sensitive buildings such as hospitals or retirement homes. But according to the latest findings, hygiene has also become an impor-
 tant topic for the construction of single- and two-family houses. In this connection, several requirements must be met by the design of drinking water installations. Only specialised companies should be involved in their planning or modification. They know all the relevant technical aspects and are obliged to adhere to them. The dimensional design of the pipe system, the types of materials used, as well as pipe insulation and minimisation of possible water stagnation in the pipes, are of great significance. Materials in contact with the drinking water may transmit undesirable substances to the drinking water. Improper design and assembly of an installation may also further the formation and growth of biofilm, which establishes optimum conditions for the growth of undesirable microorganisms such as legionellae and pseudomonads. They may become a hazard to the occupants' health. Furthermore, the distance of flow up to the tap should be as short as possible. Dead-water sections in which the water flows only rarely or does not flow at all, need to be avoided by all means.

If the influence of all these factors can be minimized as early as at the planning stage, this will make sure that the interior installations also maintain an optimum water quality. Structural components and materials that are in contact with drinking water must not affect it adversely. Planning and assembly of drinking water installations must also ensure that the comestible drinking water is conveyed under perfect hygienic conditions.

## The following lists the most important criteria that need to be observed for perfect planning and assembly of the system and optimum drinking water quality:

- Avoidance of stagnation
- Operation as intended
- Short connecting lines
- Main consumer at the end of the single-connection line
- Separation of sections that are not in use
- Correct dimensioning
- Hydraulic alignment of circulation systems
- Avoidance of cold water heating up (max. $25^{\circ} \mathrm{C}$ )
- Avoidance of hot water cooling down (min. $55^{\circ} \mathrm{C}$ )
- Expert initial operation (pressure test, flushing)


## DRINKING WATER HYGIENE

A loop line avoids stagnation in a drinking water installation from the very beginning.

Serial lines only make sense, if the last consumer is a frequently used sanitary device.
T-installations can lead to water stagnating in the lines.

### 3.2 Types of Installation

### 3.2.1 Connection of Drinking Water Tapping Points

The quality of drinking water provided in an interior installation is entirely dependent on the observance of certain temperature ranges and the avoidance of stagnation. Traditional piping networks make it almost impossible to observe both requirements under the prevailing conditions of use. Therefore, drinking water tapping points are nowadays preferably interconnected in loop lines.

Interconnection of tapping points in a loop line proves to be an effective concept of avoiding stagnating water.

Examples of different installation types:


This description is based on directives applicable in Germany and the European Union.

These are the important directives on the quality of water that is intended for consumption by humans:

- Germany: Drinking Water Ordinance (Trinkwasserverordnung TrinkwV2001)
- European Union: Directive on Drinking Water 98/83/EG

Traditional pipe installation, for example, T-systems or floor manifolds for drinking water installation in buildings, frequently causes hygienic problems because of stagnation or inadmissible heating up of cold water. However, if no other way of installation can be used, water contamination should be avoided by forced pipe flushing.

## DRINKING WATER HYGIENE

## 3．2．2 Fittings for Hygienic Piping



To provide the required drinking water quality，POLOPLAST has developed a new double wall union，which allows the types of piping indicated before to be used．

Several tapping points can now be connected，while the hygienic requirements of，for example，hotels and hospitals are fulfilled．They ensure that the entire amount of water contained in the piping is replaced at regular intervals．This prevents stagnation．

Hygienic piping is also possible using the transition wall union．

### 4.1 Standards and Regulations

## SYSTEM REQUIREMENTS

## 4．2 Terms Used

## 4．2．1 Standard Dimension Ratio

SDR is an index in use for the classification of plastic pipes，which describes the ratio between a pipe＇s outer diameter and its wall thickness．

## SDR＝ $2 \cdot S+1$ <br> SDR $\approx \frac{d_{a}}{s}$

$S=$ pipe series number
$s=$ wall thickness
da＝outer diameter
The SDR index indicates the resistance to pressure．A certain SDR index is required for every type of mate－ rial to provide a certain resistance to pressure．The required SDR index is determined by thermal load and hydrostatic load．

The following correlation applies：
－the thicker the wall，the smaller the SDR index；
－the smaller the SDR index，the higher the resistance of a pipe to pressure．

## 4．2．2 Pipe Series Number S



The nominal pipe series number is a dimensionless index，which is used for the calculation of the wall thick－ ness of pipes．

The following equation is used for the calculation of the pipe series number S ：

## $S=\frac{S D R-1}{2}$

Example：POLO－ECOSAN Pipe SDR $6=$ S 2.5 This reference value was used in the first plastic pipe standards（for example，DIN 8077 －1974／1989）and was based on a safety factor of 2．0．The maximum working pressure of 20 bar， 16 bar， 10 bar only refers to a service life of 50 years at a working temperature of $20^{\circ} \mathrm{C}$ ．However，at elevated temperatures the Maximum Operating Pressure is lower．
This circumstance frequently leads to confusion．
For an exact pipe classification under various operating conditions，newer versions of the respective standards （DIN 8077 － 1999 or EN ISO 15874 －2003）therefore only state the pipe series S or the diameter－wall thickness ratio SDR．

## SYSTEM REQUIREMENTS

### 4.3 Requirements on Pipe Systems

Standards on the various products (for PP-R: EN ISO 15874), as well as the most recent standard on multilayer pipes (DIN EN ISO 21003) have introduced the term "classification of operating conditions".

The requirements made on pipe systems over their operating time according to ISO 15874 have been defined for four classes of application and are indicated in Table 1.

An admissible working pressure of 4 bar, 6 bar, 8 bar or, respectively, 10 bar is valid for each of the different classes of application.

All systems that comply with the conditions as stated in Table 1 must be suitable for conveying cold water at $20^{\circ} \mathrm{C}$ and an admissible working pressure of 10 bar over a period of 50 years.

Only water or treated water may be used as heat transmitter in heating systems.

### 4.3.1 Classification of Operational Conditions

Class of application according to DIN EN ISO 15874
Table 1

| Class of application | Design temperature $\mathrm{T}_{\mathrm{D}}$ ${ }^{\circ} \mathrm{C}$ | Duration of operation ${ }^{\text {at }} \mathrm{T}_{\mathrm{D}}$ years | $\begin{gathered} \mathrm{T}_{\text {max }} \\ { }^{\circ} \mathrm{C} \end{gathered}$ | Duration of operation at $\mathrm{T}_{\text {max }}$ year(s) | $\begin{aligned} & \mathrm{T}_{\text {max }} \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | Duration of operation at $\mathrm{T}_{\text {times }}$ h | Typical field of application |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1^{\text {a }}$ | 60 | 49 | 80 | 1 | 95 | 100 | Hot water supply ( $60^{\circ} \mathrm{C}$ ) |
| $2^{\text {a }}$ | 70 | 49 | 80 | 1 | 95 | 100 | Hot water supply ( $70^{\circ} \mathrm{C}$ ) |
| $4^{\text {b }}$ | 20  <br> 40  <br>  Follo <br> 60  <br> Followed by (  |  2,5 <br> d by  <br>  20 <br> d by  <br>  25 <br> next column)  | 70 | $2.5$ <br> ollowed by next column) | 100 | 100 | Underfloor heating and low-temperature radiator connection |
| $5^{\text {b }}$ | 20 60 80 Follo Followed by (s | 14 <br> by <br> 25 <br> by <br> 10 <br> next column) |  | 1 <br> lowed by ext column) | 100 | 100 | High-temperature radiator connection |

Annotation: This international standard does not apply, if values that are higher than those stated in the table are taken as a basis for $T_{D}, T_{\max }$ and $T_{\text {times }}$.
a Pursuant to national regulations either class 1 or class 2 may be selected.
b If more than one design temperature is obtained for a class of application, the respective operating periods should be added up (for example, the universe of temperatures for class 5 and a duration of 50 years consists of the following:

- $20^{\circ} \mathrm{C}$ over 14 years, followed by
- $60^{\circ} \mathrm{C}$ over 25 years, followed by
- $80^{\circ} \mathrm{C}$ over 10 years, followed by
- $90^{\circ} \mathrm{C}$ over 1 years, followed by
- $100^{\circ} \mathrm{C}$ over 100 h .)


### 4.3.2 Table of Working Pressure Values

Long-term stress behaviour of POLOPLAST pipes with a safety factor of 1.25
Table 2

|  |  | $\begin{aligned} & \text { POLO-ECOSAN } \\ & \text { SDR } 6 \end{aligned}$ |  | $\begin{aligned} & \text { POLO-ECOSAN } \\ & \text { SDR } 11 \end{aligned}$ |  | $\begin{aligned} & \text { POLO-ECOSAN ML5 } \\ & \text { SDR } 7.4 \end{aligned}$ |  | POLO-UV ML5$\text { SDR } 7.4$ |  | $\begin{aligned} & \text { POLO-ECOSAN ML3 } \\ & \text { SDR } 11 \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum working pressure |  |  |  |  |  |  |  |  |  |
|  |  | bar | psi | bar | psi | bar | psi | bar | psi | bar | psi |
| $20^{\circ} \mathrm{C}$ | 1 | 36.0 | 522 | 18.0 | 261 | 31.5 | 457 | 28.5 | 413 | 19.9 | 289 |
|  | 5 | 33.8 | 490 | 16.9 | 245 | 29.6 | 429 | 26.8 | 389 | 19.3 | 280 |
|  | 10 | 32.8 | 476 | 16.4 | 238 | 28.9 | 419 | 26.1 | 379 | 19.0 | 276 |
|  | 25 | 31.8 | 461 | 16.0 | 232 | 27.9 | 405 | 25.2 | 366 | 18.6 | 270 |
|  | 50 | 30.9 | 448 | 15.5 | 225 | 27.1 | 393 | 24.5 | 355 | 18.4 | 267 |
| $30^{\circ} \mathrm{C}$ | 1 | 30.6 | 444 | 15.3 | 222 | 26.9 | 390 | 24.2 | 351 | 17.2 | 250 |
|  | 5 | 28.7 | 416 | 14.4 | 209 | 25.2 | 366 | 22.7 | 329 | 16.6 | 241 |
|  | 10 | 27.7 | 402 | 13.9 | 202 | 24.5 | 355 | 22.1 | 321 | 16.4 | 238 |
|  | 25 | 26.8 | 389 | 13.4 | 194 | 23.6 | 342 | 21.3 | 309 | 16.1 | 234 |
|  | 50 | 26.1 | 379 | 13.1 | 190 | 23.0 | 334 | 20.7 | 300 | 15.8 | 229 |
| $40^{\circ} \mathrm{C}$ | 1 | 25.8 | 374 | 12.9 | 187 | 22.8 | 331 | 20.6 | 299 | 14.8 | 215 |
|  | 5 | 24.2 | 351 | 12.1 | 176 | 21.4 | 310 | 19.2 | 279 | 14.3 | 207 |
|  | 10 | 23.6 | 342 | 11.8 | 171 | 20.8 | 302 | 18.7 | 271 | 14.1 | 205 |
|  | 25 | 22.6 | 328 | 11.3 | 164 | 20.0 | 290 | 18.0 | 261 | 13.8 | 200 |
|  | 50 | 22.0 | 319 | 11.0 | 160 | 19.4 | 281 | 17.4 | 252 | 13.6 | 197 |
| $50^{\circ} \mathrm{C}$ | 1 | 22.0 | 319 | 11.0 | 160 | 19.3 | 280 | 17.4 | 252 | 12.6 | 183 |
|  | 5 | 20.4 | 296 | 10.2 | 148 | 18.0 | 261 | 16.2 | 235 | 12.2 | 177 |
|  | 10 | 19.7 | 286 | 9.9 | 144 | 17.5 | 254 | 15.7 | 228 | 12.0 | 174 |
|  | 25 | 19.1 | 277 | 9.6 | 139 | 16.8 | 244 | 15.1 | 219 | 11.7 | 170 |
|  | 50 | 18.5 | 268 | 9.3 | 135 | 16.3 | 236 | 14.7 | 213 | 11.5 | 167 |
| $60^{\circ} \mathrm{C}$ | 1 | 18.5 | 268 | 9.3 | 135 | 16.3 | 236 | 14.7 | 213 | 10.7 | 155 |
|  | 5 | 17.2 | 250 | 8.6 | 125 | 15.2 | 220 | 13.6 | 197 | 10.3 | 149 |
|  | 10 | 16.6 | 241 | 8.3 | 120 | 14.7 | 213 | 13.2 | 191 | 10.1 | 147 |
|  | 25 | 15.9 | 231 | 8.0 | 116 | 14.1 | 205 | 12.7 | 184 | 9.9 | 144 |
|  | 50 | 15.3 | 222 | 7.7 | 112 | 13.7 | 199 | 12.3 | 178 | 9.7 | 141 |
| $70^{\circ} \mathrm{C}$ | 1 | 15.6 | 226 | 7.8 | 113 | 13.7 | 199 | 12.3 | 178 | 9.0 | 131 |
|  | 5 | 14.3 | 207 | 7.2 | 104 | 12.7 | 184 | 11.4 | 165 | 8.6 | 125 |
|  | 10 | 14.0 | 203 | 7.0 | 102 | 12.3 | 178 | 11.1 | 161 | 8.5 | 123 |
|  | 25 | 12.1 | 176 | 6.1 | 88 | 11.8 | 171 | 9.6 | 139 | 8.3 | 120 |
|  | 50 | 10.2 | 148 | 5.1 | 74 | 11.4 | 165 | 8.1 | 117 | 8.1 | 117 |
| $80^{\circ} \mathrm{C}$ | 1 | 13.1 | 190 | 6.5 | 94 | 11.5 | 167 | 10.3 | 149 | 7.5 | 109 |
|  | 5 | 11.5 | 167 | 5.7 | 83 | 10.6 | 154 | 9.1 | 132 | 7.2 | 104 |
|  | 10 | 9.6 | 139 | 4.8 | 70 | 10.2 | 148 | 7.7 | 112 | 7.0 | 102 |
|  | 25 | 7.6 | 110 | 3.8 | 55 | 9.8 | 142 | 6.2 | 90 | 6.9 | 100 |
|  | 50 | 6.4 | 93 |  |  | 9.5 | 138 | 5.3 | 77 |  |  |
| $95^{\circ} \mathrm{C}$ | 1 | 9.2 | 133 | 4.6 | 67 | 8.7 | 126 | 7.3 | 106 | 5.6 | 81 |
|  | 5 | 6.2 | 90 | 3.1 | 45 | 8.0 | 116 | 4.9 | 71 | 5.3 | 77 |
|  | 10 | 5.2 | 75 | 2.6 | 38 | 7.7 | 112 | 4.2 | 61 | 5.2 | 75 |
|  | 25 | 4.4 | 64 |  |  | 7.4 | 107 | 3.4 | 49 |  |  |

Admissible working pressure values for domestic installations (medium: water according to the Drinking Water Ordinance TrinkwV 2001)
SDR = Standard Dimension Ratio (diameter / wall thickness ratio)

## SYSTEM REQUIREMENTS

This table enables you to select the suitable pipe for your application. You should know the requirements made on the system (temperature, pressure).

## Example of how to select a pipe:

Field of application: cold water
Temperature of the medium: $20^{\circ} \mathrm{C}$
Maximum working pressure: 10 bar

Selection:
Step 1: select the applicable temperature range $>20^{\circ} \mathrm{C}$
Step 2: select the required service life $>50$ years
Step 3: maximum working pressure within the system $10 \mathrm{bar}>$ pressure according to the table > $15.5 \mathrm{bar}>$ Selection: POLO-ECOSAN pipe SDR 11

Field of application: hot water
Temperature of the medium: $70^{\circ} \mathrm{C}$
Maximum working pressure: 10 bar

## Selection:

Step 1: select the applicable temperature range $>70^{\circ} \mathrm{C}$
Step 2: select the required service life > 50 years
Step 3: maximum working pressure within the system 10 bar > pressure according to the table > 11.4 bar > Selection: POLO-ECOSAN ML5 pipe SDR 7.4

Suggestion: pipe for a maximum working pressure of 10 bar

- cold water $20^{\circ} \mathrm{C}$ : POLO-ECOSAN SDR 11
- hot water $70^{\circ} \mathrm{C}$ : POLO-ECOSAN ML5 SDR 7.4


### 4.3.3 Stress that a Pipe System is Exposed to

When planning and laying pipes, you should always take into account the following interior and exterior stress factors that the pipe system may be exposed to:

## Factors:

- Temperature (from the inside and the outside)
- Chemical stress
- Pressure (excess and negative)
- Extension (tensile and compression load)
- Exterior loads from underground laying, traffic and heavy structural components


## SYSTEM REQUIREMENTS

### 4.4 Chemical Resistance

Thanks to the special properties of its materials, the POLO-ECOSAN installation system features excellent chemical resistance.
Chemical resistance of the POLO-ECOSAN Fittings with brass inserts cannot be put on a level with the resistance of those system elements that are only made of PP-R.

Metallic copper, manganese or cobalt deteriorate the thermal ageing resistance of PP-R, above all, if the plasticized materials come into contact with these metals. Please contact POLOPLAST, if the pipe system is likely to come into contact with chemicals and other aggressive media.

Inquiry regarding the chemical resistance of the POLO-ECOSAN pipe system

| Installation company: |  |
| :--- | :--- |
|  | Firm |
|  | Contact person |
|  | Street |
|  | Postal code/Place |
|  | Telephone |


|  | Building Project |
| :--- | :--- |
|  | Street |
|  | Place |

Area of application:
Flow medium

|  | Flow medium |  |
| :---: | :---: | :---: |
|  | ${ }^{\circ} \mathrm{C}$ | Service temperature |
|  | mbar | Service pressure |
|  |  | Running time |
|  |  |  |

Place, date

[^1]
### 4.5 Disinfection

### 4.5.1 Thermal Disinfection

In proven cases of contamination, the disinfection of drinking water installations must only be carried out for a limited period of time. Prophylactic disinfection measures do not comply with the minimum quality requirements of the Drinking Water Ordinance. The disinfection of drinking water installations can only be successful, if all sources of contamination have been removed beforehand. The limit values for disinfectant concentration specified in the Drinking Water Ordinance represent maximum values, which were set in accordance with hygienic and toxicological standards. However, no conclusions should be drawn automatically from these values with regard to the resistance of product materials to the disinfectant agents. Only trained specialists may carry out the disinfection of drinking water installations. The disinfection measures must be recorded in writing.

Disinfection measures carried out incorrectly can damage the drinking water installation. A combined ther-mal-chemical disinfection procedure is not permitted.

The thermal disinfection of POLOPLAST pipe systems must be carried out as follows:

- The water heater and the entire circulation system must be heated to at least $70^{\circ} \mathrm{C}$.
- Open all draw-off points in succession or line by line.
- Hot water at a temperature of $70^{\circ} \mathrm{C}$ must be allowed to run from all draw-off points for at least three minutes.
- Do not allow the temperature to drop during the disinfection process.
- Do not exceed the maximum temperature of $95^{\circ} \mathrm{C}$.
- Take suitable measures to eliminate the risk of scalding.

The total thermal disinfection time for drinking water installations must not exceed 150 hours per year. Longer disinfection times or excessive temperatures can reduce the service life of the drinking water installation and can damage the system.

It might be necessary to carry out thermal disinfection on a regular basis to stop the growth of legionellae. Legionellae are killed at temperatures higher than $55^{\circ} \mathrm{C}$.

| Killing times | at $70^{\circ} \mathrm{C}$ | 3 min. |
| :--- | :--- | :--- |
|  | at $60^{\circ} \mathrm{C}$ | $60-120$ min. |
|  | at $55^{\circ} \mathrm{C}$ | $180-240 \mathrm{~min}$. |

To provide sufficient disinfection it must be made sure that a temperature level of more than $70^{\circ} \mathrm{C}$ is achieved within the entire system.
Provided this type of disinfection is applied on a regular basis and a constant temperature level of more than $65^{\circ} \mathrm{C}$ is guaranteed, the PP-RCT is particularly suitable, because of its improved long-term thermal resistance.

## SYSTEM REQUIREMENTS

### 4.5.2 Chemical Disinfection - "Shock Disinfection"

During the process of chemical disinfection ("shock disinfection") in accordance with Pt. 7.5.2 of the ÖNORM-Standard B 5019, the disinfecting agent can be fed into the cold water circulation or the warm water circulation, respectively. When the disinfecting agent is fed into the warm water circulation, the temperature must first be reduced to below $25^{\circ} \mathrm{C}$. Carrying out "shock disinfections" at higher temperatures is not permissible, as premature material damage cannot be ruled out. In relation to the service life of the installed system, the number of disinfecting procedures must not exceed 5 cycles. No drinking water may be drawn either during the disinfection process or during the subsequent flushing of the system with cold water.

Table 3 lists the concentration and contact times of chemicals on the basis of ÖNORM-Standard B 5019.

Table 3: Concentration and contact times of chemicals for chemical disinfection

During the application the applied concentration and application temperature may not be exceeded at any point within the pipe system.

### 4.5.3 Continuous Metered Addition of Chemicals - "Permanent Disinfection"

The continuous metered addition of chemicals according to Pt. 9 of the ÖNORM-Standard B 5019 is only permissible in instances when repeated decontamination processes (thermal, chemical, according to Section 7 of the ÖNORM-Standard) did not produce the desired results and where the systems in question have low levels of biofilm.
It must be stated that the continuous metered addition of chemicals can in no way replace the structural refurbishment of the pipe system and should be regarded merely as temporary supporting measure until such a time as the refurbishment takes place, and not as prophylactic measure against Legionella.

If the timeframe and the maximum water temperature are exceeded, damage to the component parts of the pipe systems (pipe, seals, o-rings, etc.) cannot be ruled out. This applies to all prevalent materials used in plumbing technology (types of metal, plastics and elastomers).

Table 4 lists the concentration and contact times of chemicals on the basis of ÖNORM-Standard B 5019.
Table 4
$\left.\begin{array}{|l|c|c|c|c|}\hline \text { Active component } & \text { Chemical formula } & \text { Max. concentration applied } & \text { Max. period of application } & \text { Max. water temp. in the system } \\ \hline \text { Chlorine Dioxide }{ }^{* \star} & \mathrm{ClO}_{2} & 0.4 \mathrm{mg} / \mathrm{l} \text { als ClO} \\ 2 & & 4 \text { months } & 60^{\circ} \mathrm{C} \\ \hline \text { Hypochlorite } & \mathrm{ClO}^{-} & 0.3 \mathrm{mg} / / \mathrm{als} \mathrm{Cl} \\ 2 \text { (Chlor) }\end{array}\right)$

Table 4: Concentration and contact times of chemicals for continuous metered addition
** For the disinfection process using chlorine dioxide (listed as $\mathrm{ClO}_{2}$ ) the maximum amount that can be added into the pipe system is $0.4 \mathrm{mg} / \mathrm{ClO}_{2}$.

### 5.1 Dimensioning of Drinking Water Systems

### 5.1.1 Differentiating Calculation Procedure

Planning and construction of drinking water installations are based the DIN EN 806 standard or relevant national collateral standards such as DIN 1988-300. These define the procedure used to determine the pipe diameters, which is achieved by calculating the loss of pressure in the pipe system. The pressure loss depends on the pipe length, pipe material, the type of fittings used, as well as the flow rate, which is influenced by the number and size of taps and fittings.

The following data is required to determine pressure losses and pipe diameters:

- supply pressure or outlet pressure after a pressure-reducing valve or pressure increase
- difference in geodetic altitude
- pressure loss related to fittings (e.g., water meters, filters, water softening equipment, etc.)
- minimum flow pressure at the tapping points
- loss of pressure due to the resistance of the pipe materials used
- coefficients of losses relating to fittings and connecting elements used

Below, we introduce a simplified calculation (acc. to EN 806) and a differentiating calculation procedure (acc. to DIN 1988) for the determination of the pipe diameters. The choice of alternative methods allows the selection of the most suitable method for the relevant application. The simplified calculation is recommended for small-scale projects and simple drinking water installations. However, in the interest of hygiene, the differentiating calculation procedure is preferable, in order to ensure the precise calculation and dimensioning of the installation.

The model for the differentiating calculation is illustrated in the process depicted below.

| Determine total flow rates and allocate to relevant sections <br> Starting from the farthest tapping point and leading to the supply line, the calculated flow rates are added, and the total flow rates are allocated <br> to the corresponding line sections. |  |
| :--- | :--- |
| Determine peak flow rate from the total flow rate <br> To calculate the pipeline system, all draw-off tapping points are generally assigned to their respective calculated flows. Simultaneous water <br> tapping depends on the type of use (e.g. residential or communal systems). <br> Generally, it can be assumed that not all taps will be opened at the same time. <br> For piping installations in residential buildings, the corresponding peak flow rate can be determined using the formula / diagram in DIN 1988 <br> Section 300. |  |
| Determine pressure difference for pipe resistance and individual resistance values. |  |
| Differentiating Calculation Procedure | Simplified Calculation Procedure |
| Determine pressure loss value from individual resistance values via <br> loss correction values | Calculate total pressure loss from pipe resistance of all segments and <br> compare to available pressure difference |
| Calculate total pressure loss from pipe friction and individual <br> resistance values, and compare to available pressure difference | If necessary, re-calculate using altered pipe diameters |
| If necessary, re-calculate using altered pipe diameters |  |

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For sound insulation reasons and in order to limit pressure surges, the calculated flow rate must not exceed the values provided below.

Maximum flow rate in accordance with DIN 1988-300
Table 5

| Line section | Maximum calculated flow rate for a duration of |  |  |
| :---: | :---: | :---: | :---: |
|  | connecting lines | $\leq 15 \mathrm{~min}$ | $>15 \mathrm{~min}$ |
| Supply pipes | pipe sections with pipe valve fittings featuring low <br> pressure loss $(\zeta<2.5)^{*}$ | $2 \mathrm{~m} / \mathrm{s}$ | $2 \mathrm{~m} / \mathrm{s}$ |
|  | pipe sections with pipe valve fittings with higher <br> loss coefficient values ** | $2 \mathrm{~m} / \mathrm{s}$ | $2 \mathrm{~m} / \mathrm{s}$ |

* e.g. piston slide valves acc. to DIN 3500, ball valves, slanted seat valves acc. to DIN 3502 (starting from DN 20)
** e.g. shut off valves acc. to DIN 351


### 5.1.2 Minimum Flow Pressures of Tapping Points

## Standard minimum flow pressure values and calculated flow rates for selected drinking water tapping points <br> Table 6

| Type of drinking water tapping point |  |  | Calculated flow for outlet of |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | mixed water* |  | either cold or hot drinking water |
| Minimum flow pressure $_{\text {Pmin }}$ bar |  |  | volume flow cold I/s | volume flow hot 1/s | volume flow I/s |
| 0.5 | outlet valves without aerator** | DN 15 | - | - | 0.30 |
| 0.5 |  | DN 20 | - | - | 0.50 |
| 0.5 |  | DN 25 | - | - | 1.00 |
| 1.0 | outlet valves with aerator | DN 10 | - | - | 0.15 |
| 1.0 |  | DN 15 | - | - | 0.15 |
| 1.0 | shower heads for cleaning showers |  | 0.10 | 0.10 | 0.20 |
| 1.2 | pressure flusher according to DIN 3265. part 1 | DN 15 | - | - | 0.70 |
| 1.2 | pressure flusher according to DIN 3265. part 1 | DN 20 | - | - | 1.00 |
| 0.4 | pressure flusher according to DIN 3265. part 1 | DN 25 | - | - | 1.00 |
| 1.0 | pressure flusher for urinals | DN 15 | - | - | 0.30 |
| 1.0 | household dishwasher | DN 15 | - | - | 0.15 |
| 1.0 | household washing machine | DN 15 | - | - | 0.25 |
| 1.0 | mixers for showers | DN 15 | 0.15 | 0.15 | - |
| 1.0 | mixers for bath tubs | DN 15 | 0.15 | 0.15 | - |
| 1.0 | mixers for kitchen sinks | DN 15 | 0.07 | 0.07 | - |
| 1.0 | mixers for wash basins | DN 15 | 0.07 | 0.07 | - |
| 1.0 | mixers for bidets | DN 15 | 0.07 | 0.07 | - |
| 1.0 | mixer | DN 20 | 0.30 | 0.30 | - |
| 0.5 | cistern according to DIN 19542 | DN 15 | - | - | 0.13 |
| 1.0 | electric water boiler | DN 15 | - | - | 0.10 *** |

* The calculated flow rates for the supply of mixed water are based on a temperature of $15^{\circ} \mathrm{C}$ for cold water and $60^{\circ} \mathrm{C}$ for heated drinking water.
** For outlet valves without aerator and with threaded hose connection, the pressure loss in the hose assembly (up to a length of 10 m ) and in the connected appliance (e.g. lawn sprinkler) is taken into account as a flat rate minimum flow pressure. In this case, the minimum flow pressure increases by 1.0 bar to 1.5 bar.
*** with fully opened throttle valve.
Annotation: When determining the pipe diameter, draw-off points which are not included in the table as well as valves and fittings of a similar kind with flow rates of fittings or minimum flow pressures that are greater than indicated must be taken into account as per the recommendations of the manufacturer.


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### 5.1.3 Peak Flow Rate According to DIN 1988

Simultaneous water tapping depends on the type of use (e.g. in residential buildings, hotels, etc.). Generally, it can be assumed that not all connected taps will be fully open at the same time. Consequently, the cumulative flow can be converted into the peak flow rate.

Determination of the peak flow rate $V_{S}$ from the total flow rate $\Sigma V_{R}$

## Diagram:



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## Table 7:

Values in I/s for residential buildings, offices / administration buildings with an assumed calculated flow rate of the tapping point $\mathrm{V}_{\mathrm{R}}<0.5 \mathrm{l} / \mathrm{s}$

Table 7

| $\Sigma V_{\text {R }}$ | $\mathrm{V}_{\text {s }}$ | $\Sigma V_{\text {R }}$ | $\mathrm{V}_{\text {s }}$ | $\Sigma \mathrm{V}_{\text {R }}$ | $\mathrm{V}_{\text {s }}$ | $\Sigma V_{\text {R }}$ | $\mathrm{V}_{\text {s }}$ | $\Sigma V_{\text {R }}$ | $\mathrm{V}_{\text {s }}$ | $\Sigma \mathrm{V}_{\text {R }}$ | $\mathrm{V}_{\text {s }}$ | $\Sigma V_{\text {R }}$ | $\mathrm{V}_{\text {s }}$ | $\Sigma \mathrm{V}_{\text {R }}$ | $\mathrm{V}_{\text {s }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.02 | 0.02 | 1.02 | 0.55 | 2.02 | 0.80 | 3.02 | 0.98 | 4.02 | 1.14 | 5.10 | 1.28 | 10.10 | 1.79 | 15.10 | 2.17 |
| 0.04 | 0.04 | 1.04 | 0.55 | 2.04 | 0.80 | 3.04 | 0.98 | 4.04 | 1.14 | 5.20 | 1.29 | 10.20 | 1.80 | 15.20 | 2.18 |
| 0.06 | 0.06 | 1.06 | 0.56 | 2.06 | 0.80 | 3.06 | 0.99 | 4.06 | 1.14 | 5.30 | 1.30 | 10.30 | 1.81 | 15.30 | 2.19 |
| 0.08 | 0.08 | 1.08 | 0.57 | 2.08 | 0.81 | 3.08 | 0.99 | 4.08 | 1.14 | 5.40 | 1.32 | 10.40 | 1.82 | 15.40 | 2.19 |
| 0.10 | 0.10 | 1.10 | 0.57 | 2.10 | 0.81 | 3.10 | 0.99 | 4.10 | 1.15 | 5.50 | 1.33 | 10.50 | 1.82 | 15.50 | 2.20 |
| 0.12 | 0.12 | 1.12 | 0.58 | 2.12 | 0.82 | 3.12 | 1.00 | 4.12 | 1.15 | 5.60 | 1.34 | 10.60 | 1.83 | 15.60 | 2.21 |
| 0.14 | 0.14 | 1.14 | 0.58 | 2.14 | 0.82 | 3.14 | 1.00 | 4.14 | 1.15 | 5.70 | 1.35 | 10.70 | 1.84 | 15.70 | 2.21 |
| 0.16 | 0.16 | 1.16 | 0.59 | 2.16 | 0.82 | 3.16 | 1.00 | 4.16 | 1.16 | 5.80 | 1.36 | 10.80 | 1.85 | 15.80 | 2.22 |
| 0.18 | 0.18 | 1.18 | 0.59 | 2.18 | 0.83 | 3.18 | 1.01 | 4.18 | 1.16 | 5.90 | 1.38 | 10.90 | 1.86 | 15.90 | 2.23 |
| 0.20 | 0.19 | 1.20 | 0.60 | 2.20 | 0.83 | 3.20 | 1.01 | 4.20 | 1.16 | 6.00 | 1.39 | 11.00 | 1.87 | 16.00 | 2.23 |
| 0.22 | 0.21 | 1.22 | 0.61 | 2.22 | 0.84 | 3.22 | 1.01 | 4.22 | 1.16 | 6.10 | 1.40 | 11.10 | 1.87 | 16.10 | 2.24 |
| 0.24 | 0.22 | 1.24 | 0.61 | 2.24 | 0.84 | 3.24 | 1.02 | 4.24 | 1.17 | 6.20 | 1.41 | 11.20 | 1.88 | 16.20 | 2.25 |
| 0.26 | 0.23 | 1.26 | 0.62 | 2.26 | 0.84 | 3.26 | 1.02 | 4.26 | 1.17 | 6.30 | 1.42 | 11.30 | 1.89 | 16.30 | 2.25 |
| 0.28 | 0.24 | 1.28 | 0.62 | 2.28 | 0.85 | 3.28 | 1.02 | 4.28 | 1.17 | 6.40 | 1.43 | 11.40 | 1.90 | 16.40 | 2.26 |
| 0.30 | 0.26 | 1.30 | 0.63 | 2.30 | 0.85 | 3.30 | 1.03 | 4.30 | 1.17 | 6.50 | 1.44 | 11.50 | 1.91 | 16.50 | 2.27 |
| 0.32 | 0.27 | 1.32 | 0.63 | 2.32 | 0.86 | 3.32 | 1.03 | 4.32 | 1.18 | 6.60 | 1.45 | 11.60 | 1.91 | 16.60 | 2.27 |
| 0.34 | 0.28 | 1.34 | 0.64 | 2.34 | 0.86 | 3.34 | 1.03 | 4.34 | 1.18 | 6.70 | 1.47 | 11.70 | 1.92 | 16.70 | 2.28 |
| 0.36 | 0.29 | 1.36 | 0.64 | 2.36 | 0.86 | 3.36 | 1.04 | 4.36 | 1.18 | 6.80 | 1.48 | 11.80 | 1.93 | 16.80 | 2.29 |
| 0.38 | 0.30 | 1.38 | 0.65 | 2.38 | 0.87 | 3.38 | 1.04 | 4.38 | 1.19 | 6.90 | 1.49 | 11.90 | 1.94 | 16.90 | 2.29 |
| 0.40 | 0.31 | 1.40 | 0.65 | 2.40 | 0.87 | 3.40 | 1.04 | 4.40 | 1.19 | 7.00 | 1.50 | 12.00 | 1.95 | 17.00 | 2.30 |
| 0.42 | 0.32 | 1.42 | 0.66 | 2.42 | 0.88 | 3.42 | 1.05 | 4.42 | 1.19 | 7.10 | 1.51 | 12.10 | 1.95 | 17.10 | 2.31 |
| 0.44 | 0.33 | 1.44 | 0.66 | 2.44 | 0.88 | 3.44 | 1.05 | 4.44 | 1.19 | 7.20 | 1.52 | 12.20 | 1.96 | 17.20 | 2.31 |
| 0.46 | 0.34 | 1.46 | 0.67 | 2.46 | 0.88 | 3.46 | 1.05 | 4.46 | 1.20 | 7.30 | 1.53 | 12.30 | 1.97 | 17.30 | 2.32 |
| 0.48 | 0.35 | 1.48 | 0.67 | 2.48 | 0.89 | 3.48 | 1.06 | 4.48 | 1.20 | 7.40 | 1.54 | 12.40 | 1.98 | 17.40 | 2.33 |
| 0.50 | 0.36 | 1.50 | 0.68 | 2.50 | 0.89 | 3.50 | 1.06 | 4.50 | 1.20 | 7.50 | 1.55 | 12.50 | 1.99 | 17.50 | 2.33 |
| 0.52 | 0.37 | 1.52 | 0.68 | 2.52 | 0.89 | 3.52 | 1.06 | 4.52 | 1.20 | 7.60 | 1.56 | 12.60 | 1.99 | 17.60 | 2.34 |
| 0.54 | 0.38 | 1.54 | 0.69 | 2.54 | 0.90 | 3.54 | 1.06 | 4.54 | 1.21 | 7.70 | 1.57 | 12.70 | 2.00 | 17.70 | 2.35 |
| 0.56 | 0.39 | 1.56 | 0.69 | 2.56 | 0.90 | 3.56 | 1.07 | 4.56 | 1.21 | 7.80 | 1.58 | 12.80 | 2.01 | 17.80 | 2.35 |
| 0.58 | 0.39 | 1.58 | 0.70 | 2.58 | 0.90 | 3.58 | 1.07 | 4.58 | 1.21 | 7.90 | 1.59 | 12.90 | 2.02 | 17.90 | 2.36 |
| 0.60 | 0.40 | 1.60 | 0.70 | 2.60 | 0.91 | 3.60 | 1.07 | 4.60 | 1.22 | 8.00 | 1.60 | 13.00 | 2.02 | 18.00 | 2.36 |
| 0.62 | 0.41 | 1.62 | 0.71 | 2.62 | 0.91 | 3.62 | 1.08 | 4.62 | 1.22 | 8.10 | 1.61 | 13.10 | 2.03 | 18.10 | 2.37 |
| 0.64 | 0.42 | 1.64 | 0.71 | 2.64 | 0.92 | 3.64 | 1.08 | 4.64 | 1.22 | 8.20 | 1.62 | 13.20 | 2.04 | 18.20 | 2.38 |
| 0.66 | 0.43 | 1.66 | 0.72 | 2.66 | 0.92 | 3.66 | 1.08 | 4.66 | 1.22 | 8.30 | 1.63 | 13.30 | 2.05 | 18.30 | 2.38 |
| 0.68 | 0.43 | 1.68 | 0.72 | 2.68 | 0.92 | 3.68 | 1.09 | 4.68 | 1.23 | 8.40 | 1.64 | 13.40 | 2.05 | 18.40 | 2.39 |
| 0.70 | 0.44 | 1.70 | 0.73 | 2.70 | 0.93 | 3.70 | 1.09 | 4.70 | 1.23 | 8.50 | 1.65 | 13.50 | 2.06 | 18.50 | 2.40 |
| 0.72 | 0.45 | 1.72 | 0.73 | 2.72 | 0.93 | 3.72 | 1.09 | 4.72 | 1.23 | 8.60 | 1.66 | 13.60 | 2.07 | 18.60 | 2.40 |
| 0.74 | 0.46 | 1.74 | 0.74 | 2.74 | 0.93 | 3.74 | 1.09 | 4.74 | 1.23 | 8.70 | 1.67 | 13.70 | 2.07 | 18.70 | 2.41 |
| 0.76 | 0.46 | 1.76 | 0.74 | 2.76 | 0.94 | 3.76 | 1.10 | 4.76 | 1.24 | 8.80 | 1.67 | 13.80 | 2.08 | 18.80 | 2.41 |
| 0.78 | 0.47 | 1.78 | 0.74 | 2.78 | 0.94 | 3.78 | 1.10 | 4.78 | 1.24 | 8.90 | 1.68 | 13.90 | 2.09 | 18.90 | 2.42 |
| 0.80 | 0.48 | 1.80 | 0.75 | 2.80 | 0.94 | 3.80 | 1.10 | 4.80 | 1.24 | 9.00 | 1.69 | 14.00 | 2.10 | 19.00 | 2.43 |
| 0.82 | 0.48 | 1.82 | 0.75 | 2.82 | 0.95 | 3.82 | 1.11 | 4.82 | 1.24 | 9.10 | 1.70 | 14.10 | 2.10 | 19.10 | 2.43 |
| 0.84 | 0.49 | 1.84 | 0.76 | 2.84 | 0.95 | 3.84 | 1.11 | 4.84 | 1.25 | 9.20 | 1.71 | 14.20 | 2.11 | 19.20 | 2.44 |
| 0.86 | 0.50 | 1.86 | 0.76 | 2.86 | 0.95 | 3.86 | 1.11 | 4.86 | 1.25 | 9.30 | 1.72 | 14.30 | 2.12 | 19.30 | 2.44 |
| 0.88 | 0.50 | 1.88 | 0.77 | 2.88 | 0.96 | 3.88 | 1.12 | 4.88 | 1.25 | 9.40 | 1.73 | 14.40 | 2.12 | 19.40 | 2.45 |
| 0.90 | 0.51 | 1.90 | 0.77 | 2.90 | 0.96 | 3.90 | 1.12 | 4.90 | 1.25 | 9.50 | 1.74 | 14.50 | 2.13 | 19.50 | 2.46 |
| 0.92 | 0.52 | 1.92 | 0.77 | 2.92 | 0.96 | 3.92 | 1.12 | 4.92 | 1.26 | 9.60 | 1.75 | 14.60 | 2.14 | 19.60 | 2.46 |
| 0.94 | 0.52 | 1.94 | 0.78 | 2.94 | 0.97 | 3.94 | 1.12 | 4.94 | 1.26 | 9.70 | 1.76 | 14.70 | 2.15 | 19.70 | 2.47 |
| 0.96 | 0.53 | 1.96 | 0.78 | 2.96 | 0.97 | 3.96 | 1.13 | 4.96 | 1.26 | 9.80 | 1.76 | 14.80 | 2.15 | 19.80 | 2.47 |
| 0.98 | 0.54 | 1.98 | 0.79 | 2.98 | 0.97 | 3.98 | 1.13 | 4.98 | 1.26 | 9.90 | 1.77 | 14.90 | 2.16 | 19.90 | 2.48 |
| 1.00 | 0.5 | 2.00 | 0.7 | 3.0 | 0.98 | 4.00 | 1.13 | 5.00 | 1.27 | 10.00 | 1.78 | 15.00 | 2.17 | 20.00 | 2.49 |

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### 5.1.4 Single Resistance Values $\zeta$

Coefficient of resistance values for fittings made of PP-R
Table 8

| Fitting Individual resistance | Graphic symbol | Remark | Resistance coefficient value $\zeta$ |
| :---: | :---: | :---: | :---: |
| Tee | $\overrightarrow{{ }_{\\| V}} \overrightarrow{ }$ | branching, dividing flow | 1.3 |
|  | $\Rightarrow \stackrel{V}{\\|}$ | passage for dividing flow | 0.3 |
|  | $\stackrel{-}{v+1}$ | counter current for dividing flow | 1.4 |
|  | $\stackrel{n+1}{=}$ | branching, merging flow | 1.3 |
|  | $\stackrel{\\|}{=}=$ | passage for merging flow | 2.5 |
|  | $\stackrel{v}{\\|}=$ | counter current for merging flow | 3.0 |
| Elbow $90^{\circ}$ | $\stackrel{\underline{V}}{\square}$ |  | 1.2 |
| Elbow 45 ${ }^{\circ}$ | vtl |  | 0.7 |
| Socket | $\left.\Rightarrow\right\|_{\vec{V}}$ |  | 0.25 |
| Reducer | $\leftrightarrows \frac{\vec{r}}{}$ | by 1 dimension | 0.4 |
|  |  | by 2 dimensions | 0.6 |
|  |  | by 3 dimensions | 0.7 |
|  |  | more than 4 dimensions | 0.9 |
| Wall union | ${ }_{v t} \Gamma^{\lceil }$ |  | 1.7 |
| Double wall union | $t \aleph_{v}^{[ }$ |  | 1.5 |
| Short cross over | - |  | 1.9 |
| Transition with internal thread | $\xrightarrow{\rightarrow}$ |  | 0.5 |
| Transition with internal thread, reduced | " |  | 0.8 |
| Transition with external thread | $\underset{\sim}{\square}$ |  | 0.4 |
| Transition with external thread, reduced |  |  | 0.8 |
| Transition elbow with thread | + ${ }^{\text {c }}$ |  | 1.7 |
| Tee with transition, dividing flow | $\rightarrow \underset{\perp}{ } \rightarrow$ |  | 1.6 |
| Slanted seat valve | $\rightarrow-$ |  | 3.0 |
| Slanted seat valve with back-flow prevention | $\rightarrow$ |  | 3.8 |
| Shut off valve | ---Der-- |  | 7.0 |
| Ball valve | ---Los-- |  | 0.4 |

## PLANNING AND DESIGN

### 5.1.5 Pressure Loss Tables

Pressure loss due to pipe resistance R and flow rate v depending on flow V
Pipe SDR 6
Temperature $20^{\circ} \mathrm{C} \quad$ Roughness: $0.007 \mathrm{~mm} \quad$ Density: $998.29 \mathrm{~kg} / \mathrm{m}^{3} \quad$ Kin. viscosity: $1.004 \mathrm{E}-06 \mathrm{~m}^{2} / \mathrm{s}$

|  |  | Dimension | 16 mm | 20 mm | 25 mm | 32 mm | 40 mm | 50 mm | 63 mm | 75 mm | 90 mm | 110 mm | 125 mm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Wall thickness | 2.7 mm | 3.4 mm | 4.2 mm | 5.4 mm | 6.7 mm | 8.3 mm | 10.5 mm | 12.5 mm | 15.0 mm | 18.3 mm | 20.8 mm |
| 1/s | $\mathrm{m}^{3} / \mathrm{h}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| 0.01 | 0.04 | R in mbar/m $v$ in m/s | $\begin{gathered} 0.41 \\ 0.11 \end{gathered}$ | $\begin{aligned} & 0.15 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.03 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.02 \end{aligned}$ |  |  |  |  |  |  |
| 0.02 | 0.07 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{aligned} & 1.24 \\ & 0.23 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0.45 \\ 0.15 \\ \hline \end{array}$ | $\begin{aligned} & 0.16 \\ & 0.09 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.04 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.02 \end{aligned}$ |  |  |  |  |  |
| 0.03 | 0.11 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 2.41 \\ & 0.34 \end{aligned}$ | $\begin{aligned} & 0.87 \\ & 0.22 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0.30 \\ 0.14 \end{array}$ | $\begin{aligned} & 0.10 \\ & 0.08 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.03 \\ & 0.05 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.03 \end{aligned}$ |  |  |  |  |  |
| 0.04 | 0.14 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{aligned} & 3.89 \\ & 0.45 \end{aligned}$ | $\begin{aligned} & 1.39 \\ & 0.29 \end{aligned}$ | $\begin{array}{r} 0.48 \\ 0.18 \end{array}$ | $\begin{aligned} & 0.15 \\ & 0.11 \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.03 \end{aligned}$ |  |  |  |  |
| 0.05 | 0.18 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 5.66 \\ & 0.57 \end{aligned}$ | $\begin{aligned} & 2.02 \\ & 0.37 \end{aligned}$ | $\begin{aligned} & 0.69 \\ & 0.23 \end{aligned}$ | $\begin{gathered} 0.22 \\ 0.14 \end{gathered}$ | $\begin{aligned} & 0.08 \\ & 0.09 \end{aligned}$ | $\begin{aligned} & 0.03 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |  |  |
| 0.06 | 0.22 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{aligned} & 7.70 \\ & 0.68 \end{aligned}$ | $\begin{aligned} & 2.74 \\ & 0.44 \end{aligned}$ | $\begin{aligned} & 0.94 \\ & 0.28 \end{aligned}$ | $\begin{gathered} 0.30 \\ 0.17 \end{gathered}$ | $\begin{aligned} & 0.10 \\ & 0.11 \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.03 \end{aligned}$ |  |  |  |
| 0.07 | 0.25 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 10.02 \\ 0.79 \end{array}$ | $\begin{aligned} & 3.55 \\ & 0.51 \end{aligned}$ | $\begin{aligned} & 1.21 \\ & 0.32 \end{aligned}$ | $\begin{aligned} & 0.39 \\ & 0.20 \end{aligned}$ | $\begin{aligned} & 0.13 \\ & 0.13 \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.08 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |  |
| 0.08 | 0.29 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 12.59 \\ 0.91 \end{array}$ | $\begin{aligned} & 4.46 \\ & 0.58 \end{aligned}$ | $\begin{aligned} & 1.51 \\ & 0.37 \end{aligned}$ | $\begin{aligned} & 0.48 \\ & 0.23 \end{aligned}$ | $\begin{aligned} & 0.17 \\ & 0.14 \end{aligned}$ | $\begin{aligned} & 0.06 \\ & 0.09 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |  |
| 0.09 | 0.32 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 15.43 \\ 1.02 \end{array}$ | $\begin{aligned} & 5.45 \\ & 0.66 \end{aligned}$ | $\begin{aligned} & 1.85 \\ & 0.42 \end{aligned}$ | $\begin{aligned} & 0.59 \\ & 0.25 \end{aligned}$ | $\begin{array}{r} 0.20 \\ 0.16 \end{array}$ | $\begin{aligned} & 0.07 \\ & 0.10 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ |  |  |  |
| 0.10 | 0.36 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 18.52 \\ 1.13 \end{array}$ | $\begin{aligned} & 6.52 \\ & 0.73 \end{aligned}$ | $\begin{aligned} & 2.21 \\ & 0.46 \end{aligned}$ | $\begin{aligned} & 0.70 \\ & 0.28 \end{aligned}$ | $\begin{aligned} & 0.24 \\ & 0.18 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0.08 \\ 0.11 \\ \hline \end{array}$ | $\begin{aligned} & 0.03 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |
| 0.12 | 0.43 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 25.44 \\ 1.36 \\ \hline \end{array}$ | $\begin{aligned} & 8.92 \\ & 0.88 \end{aligned}$ | $\begin{aligned} & 3.01 \\ & 0.55 \end{aligned}$ | $\begin{aligned} & 0.95 \\ & 0.34 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.33 \\ & 0.22 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.11 \\ & 0.14 \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.09 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |
| 0.14 | 0.50 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 33.33 \\ 1.59 \\ \hline \end{array}$ | $\begin{array}{r} 11.66 \\ 1.02 \end{array}$ | $\begin{aligned} & 3.92 \\ & 0.65 \end{aligned}$ | $\begin{aligned} & 1.23 \\ & 0.40 \end{aligned}$ | $\begin{aligned} & 0.42 \\ & 0.25 \end{aligned}$ | $\begin{aligned} & 0.15 \\ & 0.16 \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.10 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ |  |  |
| 0.16 | 0.58 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 42.17 \\ 1.81 \end{array}$ | $\begin{array}{r} 14.71 \\ 1.17 \end{array}$ | $\begin{aligned} & 4.93 \\ & 0.74 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.55 \\ & 0.45 \end{aligned}$ | $\begin{aligned} & 0.53 \\ & 0.29 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.18 \\ & 0.18 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0.06 \\ 0.12 \end{array}$ | $\begin{aligned} & 0.03 \\ & 0.08 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.06 \end{aligned}$ |  |  |
| 0.18 | 0.65 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 51.96 \\ 2.04 \end{array}$ | $\begin{array}{r} 18.07 \\ 1.32 \\ \hline \end{array}$ | $\begin{aligned} & 6.05 \\ & 0.83 \end{aligned}$ | $\begin{aligned} & 1.89 \\ & 0.51 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.65 \\ & 0.32 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.22 \\ & 0.21 \end{aligned}$ | $\begin{array}{r} 0.08 \\ 0.13 \end{array}$ | $\begin{aligned} & 0.03 \\ & 0.09 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |
| 0.20 | 0.72 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 62.68 \\ 2.27 \end{array}$ | $\begin{array}{r} 21.75 \\ 1.46 \end{array}$ | $\begin{aligned} & 7.26 \\ & 0.92 \end{aligned}$ | $\begin{aligned} & 2.27 \\ & 0.57 \end{aligned}$ | $\begin{aligned} & 0.78 \\ & 0.36 \end{aligned}$ | $\begin{aligned} & 0.27 \\ & 0.23 \end{aligned}$ | $\begin{array}{r} 0.09 \\ 0.14 \end{array}$ | $\begin{array}{r} 0.04 \\ 0.10 \end{array}$ | $\begin{aligned} & 0.02 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ |  |
| 0.30 | 1.08 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 129.98 \\ 3.40 \end{array}$ | $\begin{array}{r} 44.65 \\ 2.19 \end{array}$ | $\begin{array}{r} 14.77 \\ 1.39 \end{array}$ | $\begin{aligned} & 4.58 \\ & 0.85 \end{aligned}$ | $\begin{aligned} & 1.56 \\ & 0.54 \end{aligned}$ | $\begin{aligned} & 0.53 \\ & 0.34 \end{aligned}$ | $\begin{aligned} & 0.18 \\ & 0.22 \end{aligned}$ | $\begin{aligned} & 0.08 \\ & 0.15 \end{aligned}$ | $\begin{aligned} & 0.03 \\ & 0.11 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ |
| 0.40 | 1.44 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 219.69 \\ 4.53 \end{array}$ | $\begin{array}{r} 74.89 \\ 2.92 \end{array}$ | $\begin{array}{r} 24.60 \\ 1.85 \end{array}$ | $\begin{aligned} & 7.58 \\ & 1.13 \end{aligned}$ | $\begin{aligned} & 2.56 \\ & 0.72 \end{aligned}$ | $\begin{aligned} & 0.87 \\ & 0.46 \end{aligned}$ | $\begin{aligned} & 0.29 \\ & 0.29 \end{aligned}$ | $\begin{aligned} & 0.13 \\ & 0.20 \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.14 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.09 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.07 \end{aligned}$ |
| 0.50 | 1.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 331.49 \\ 5.67 \end{array}$ | $\begin{array}{r} 112.32 \\ 3.65 \end{array}$ | $\begin{array}{r} 36.68 \\ 2.31 \end{array}$ | $\begin{array}{r} 11.24 \\ 1.42 \end{array}$ | $\begin{aligned} & 3.78 \\ & 0.90 \end{aligned}$ | $\begin{aligned} & 1.28 \\ & 0.57 \end{aligned}$ | $\begin{aligned} & 0.43 \\ & 0.36 \end{aligned}$ | $\begin{aligned} & 0.19 \\ & 0.25 \end{aligned}$ | $\begin{aligned} & 0.08 \\ & 0.18 \end{aligned}$ | $\begin{array}{r} 0.03 \\ 0.12 \end{array}$ | $\begin{aligned} & 0.02 \\ & 0.09 \end{aligned}$ |
| 0.60 | 2.16 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 465.18 \\ 6.80 \\ \hline \end{array}$ | $\begin{array}{r} 156.82 \\ 4.38 \\ \hline \end{array}$ | $\begin{array}{r} 50.97 \\ 2.77 \end{array}$ | $\begin{array}{r} 15.55 \\ 1.70 \\ \hline \end{array}$ | $\begin{aligned} & 5.21 \\ & 1.08 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.76 \\ & 0.68 \end{aligned}$ | $\begin{aligned} & 0.59 \\ & 0.43 \end{aligned}$ | $\begin{aligned} & 0.26 \\ & 0.31 \end{aligned}$ | $\begin{aligned} & 0.11 \\ & 0.21 \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.14 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0.02 \\ 0.11 \end{array}$ |
| 0.70 | 2.52 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 620.65 \\ 7.93 \\ \hline \end{array}$ | $\begin{array}{r} 208.34 \\ 5.12 \\ \hline \end{array}$ | $\begin{array}{r} 67.43 \\ 3.23 \\ \hline \end{array}$ | $\begin{array}{r} 20.49 \\ 1.98 \\ \hline \end{array}$ | $\begin{aligned} & 6.85 \\ & 1.26 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.30 \\ & 0.80 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.77 \\ & 0.51 \end{aligned}$ | $\begin{aligned} & 0.34 \\ & 0.36 \end{aligned}$ | $\begin{aligned} & 0.14 \\ & 0.25 \\ & \hline \end{aligned}$ | $\begin{gathered} 0.05 \\ 0.17 \\ \hline \end{gathered}$ | $\begin{array}{r} 0.03 \\ 0.13 \\ \hline \end{array}$ |
| 0.80 | 2.88 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 797.84 \\ 9.07 \end{array}$ | $\begin{array}{r} 266.84 \\ 5.85 \end{array}$ | $\begin{array}{r} 86.05 \\ 3.70 \end{array}$ | $\begin{array}{r} 26.05 \\ 2.27 \end{array}$ | $\begin{aligned} & 8.68 \\ & 1.44 \end{aligned}$ | $\begin{aligned} & 2.91 \\ & 0.91 \end{aligned}$ | $\begin{aligned} & 0.97 \\ & 0.58 \end{aligned}$ | $\begin{aligned} & 0.42 \\ & 0.41 \end{aligned}$ | $\begin{aligned} & 0.18 \\ & 0.28 \end{aligned}$ | $\begin{gathered} 0.07 \\ 0.19 \end{gathered}$ | $\begin{aligned} & 0.04 \\ & 0.15 \end{aligned}$ |
| 0.90 | 3.24 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 996.69 \\ 10.20 \end{array}$ | $\begin{array}{r} 332.29 \\ 6.58 \end{array}$ | $\begin{array}{r} 106.80 \\ 4.16 \end{array}$ | $\begin{array}{r} 32.22 \\ 2.55 \end{array}$ | $\begin{array}{r} 10.72 \\ 1.62 \end{array}$ | $\begin{aligned} & 3.58 \\ & 1.03 \end{aligned}$ | $\begin{aligned} & 1.20 \\ & 0.65 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 0.46 \end{aligned}$ | $\begin{aligned} & 0.22 \\ & 0.32 \end{aligned}$ | $\begin{aligned} & 0.08 \\ & 0.21 \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.16 \end{aligned}$ |
| 1.00 | 3.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  | $\begin{array}{r} 404.65 \\ 7.31 \end{array}$ | $\begin{array}{r} 129.67 \\ 4.62 \end{array}$ | $\begin{array}{r} 39.01 \\ 2.83 \end{array}$ | $\begin{array}{r} 12.94 \\ 1.80 \end{array}$ | $\begin{array}{r} 4.32 \\ 1.14 \end{array}$ | $\begin{aligned} & 1.44 \\ & 0.72 \end{aligned}$ | $\begin{aligned} & 0.63 \\ & 0.51 \end{aligned}$ | $\begin{aligned} & 0.26 \\ & 0.35 \end{aligned}$ | $\begin{aligned} & 0.10 \\ & 0.24 \end{aligned}$ | $\begin{aligned} & 0.06 \\ & 0.18 \end{aligned}$ |
| 1.10 | 3.96 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  | $\begin{array}{r} 483.92 \\ 8.04 \end{array}$ | $\begin{array}{r} 154.66 \\ 5.08 \end{array}$ | $\begin{array}{r} 46.40 \\ 3.12 \end{array}$ | $\begin{array}{r} 15.36 \\ 1.98 \end{array}$ | $\begin{aligned} & 5.11 \\ & 1.26 \end{aligned}$ | $\begin{aligned} & 1.70 \\ & 0.79 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.74 \\ & 0.56 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.31 \\ & 0.39 \end{aligned}$ | $\begin{aligned} & 0.12 \\ & 0.26 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.07 \\ & 0.20 \\ & \hline \end{aligned}$ |
| 1.20 | 4.32 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  | $\begin{array}{r} 570.09 \\ 8.77 \end{array}$ | $\begin{array}{r} 181.75 \\ 5.54 \end{array}$ | $\begin{array}{r} 54.40 \\ 3.40 \end{array}$ | $\begin{array}{r} 17.97 \\ 2.16 \end{array}$ | $\begin{aligned} & 5.97 \\ & 1.37 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.98 \\ & 0.87 \end{aligned}$ | $\begin{aligned} & 0.86 \\ & 0.61 \end{aligned}$ | $\begin{aligned} & 0.36 \\ & 0.42 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.14 \\ & 0.28 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.08 \\ & 0.22 \\ & \hline \end{aligned}$ |
| 1.30 | 4.68 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  | $\begin{array}{r} 663.13 \\ 9.50 \end{array}$ | $\begin{array}{r} 210.95 \\ 6.01 \end{array}$ | $\begin{array}{r} 62.99 \\ 3.68 \\ \hline \end{array}$ | $\begin{array}{r} 20.77 \\ 2.34 \\ \hline \end{array}$ | $\begin{aligned} & 6.89 \\ & 1.48 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.29 \\ & 0.94 \end{aligned}$ | $\begin{aligned} & 0.99 \\ & 0.66 \end{aligned}$ | $\begin{aligned} & 0.42 \\ & 0.46 \end{aligned}$ | $\begin{aligned} & 0.16 \\ & 0.31 \end{aligned}$ | $\begin{aligned} & 0.09 \\ & 0.24 \end{aligned}$ |
| 1.40 | 5.04 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  | $\begin{array}{r} 763.06 \\ 10.23 \end{array}$ | $\begin{array}{r} 242.24 \\ 6.47 \end{array}$ | $\begin{array}{r} 72.18 \\ 3.97 \end{array}$ | $\begin{array}{r} 23.75 \\ 2.52 \end{array}$ | $\begin{aligned} & 7.86 \\ & 1.60 \end{aligned}$ | $\begin{aligned} & 2.61 \\ & 1.01 \end{aligned}$ | $\begin{aligned} & 1.13 \\ & 0.71 \end{aligned}$ | $\begin{aligned} & 0.47 \\ & 0.50 \end{aligned}$ | $\begin{aligned} & 0.18 \\ & 0.33 \end{aligned}$ | $\begin{aligned} & 0.10 \\ & 0.26 \end{aligned}$ |
| 1.60 | 5.76 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  | $\begin{array}{r} 311.09 \\ 7.39 \end{array}$ | $\begin{array}{r} 92.33 \\ 4.53 \end{array}$ | $\begin{array}{r} 30.28 \\ 2.88 \end{array}$ | $\begin{array}{r} 10.00 \\ 1.83 \\ \hline \end{array}$ | $\begin{array}{r} 3.31 \\ 1.15 \\ \hline \end{array}$ | $\begin{aligned} & 1.43 \\ & 0.81 \end{aligned}$ | $\begin{aligned} & 0.60 \\ & 0.57 \end{aligned}$ | $\begin{aligned} & 0.23 \\ & 0.38 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.12 \\ & 0.29 \end{aligned}$ |
| 1.80 | 6.48 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  | $\begin{array}{r} 388.29 \\ 8.32 \\ \hline \end{array}$ | $\begin{array}{r} 114.85 \\ 5.10 \\ \hline \end{array}$ | $\begin{array}{r} 37.56 \\ 3.24 \end{array}$ | $\begin{array}{r} 12.37 \\ 2.05 \end{array}$ | $\begin{aligned} & 4.08 \\ & 1.30 \end{aligned}$ | $\begin{aligned} & 1.76 \\ & 0.92 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.74 \\ & 0.64 \end{aligned}$ | $\begin{aligned} & 0.28 \\ & 0.43 \end{aligned}$ | $\begin{aligned} & 0.15 \\ & 0.33 \end{aligned}$ |
| 2.00 | 7.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  | $\begin{array}{r} 473.81 \\ 9.24 \\ \hline \end{array}$ | $\begin{array}{r} 139.72 \\ 5.67 \\ \hline \end{array}$ | $\begin{array}{r} 45.56 \\ 3.60 \end{array}$ | $\begin{array}{r} 14.97 \\ 2.28 \end{array}$ | $\begin{aligned} & 4.93 \\ & 1.44 \end{aligned}$ | $\begin{aligned} & 2.13 \\ & 1.02 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.89 \\ & 0.71 \end{aligned}$ | $\begin{aligned} & 0.34 \\ & 0.47 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.18 \\ & 0.37 \\ & \hline \end{aligned}$ |
| 2.20 | 7.92 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  | $\begin{array}{r} 567.64 \\ 10.17 \\ \hline \end{array}$ | $\begin{array}{r} 166.93 \\ 6.23 \\ \hline \end{array}$ | $\begin{array}{r} 54.30 \\ 3.96 \end{array}$ | $\begin{array}{r} 17.80 \\ 2.51 \end{array}$ | $\begin{aligned} & 5.85 \\ & 1.59 \end{aligned}$ | $\begin{array}{r} 2.52 \\ 1.12 \end{array}$ | $\begin{aligned} & 1.05 \\ & 0.78 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.40 \\ & 0.52 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.22 \\ & 0.40 \\ & \hline \end{aligned}$ |
| 2.40 | 8.64 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  | $\begin{array}{r} 196.48 \\ 6.80 \end{array}$ | $\begin{array}{r} 63.77 \\ 4.32 \end{array}$ | $\begin{array}{r} 20.85 \\ 2.74 \end{array}$ | $\begin{aligned} & 6.84 \\ & 1.73 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.94 \\ & 1.22 \end{aligned}$ | $\begin{aligned} & 1.22 \\ & 0.85 \end{aligned}$ | $\begin{aligned} & 0.47 \\ & 0.57 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.25 \\ & 0.44 \\ & \hline \end{aligned}$ |

Table 9

## PLANNING AND DESIGN



## PLANNING AND DESIGN

## Pressure loss due to pipe resistance R and flow rate v depending on flow V

Pipes SDR 7,4
Temperature $20^{\circ} \mathrm{C} \quad$ Roughness: $0.007 \mathrm{~mm} \quad$ Density: $998.29 \mathrm{~kg} / \mathrm{m}^{3} \quad$ Kin. viscosity: $1.004 \mathrm{E}-06 \mathrm{~m}^{2} / \mathrm{s}$

|  |  | Dimension | 16 mm | 20 mm | 25 mm | 32 mm | 40 mm | 50 mm | 63 mm | 75 mm | 90 mm | 110 mm | 25 mm | 60 mm | 200 mm | 250 mm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Wall thickness | 2.2 mm | 2.8 mm | 3.5 mm | 4.4 mm | 5.5 mm | 6.9 mm | 8.6 mm | 10.3 mm | 12.3 mm | 15.1 mm | 17.1 mm | 21.6 mm | 27.4 mm | 34.2 mm |
| 1/s | $\mathrm{m}^{3} / \mathrm{h}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0.01 | 0.04 | R in mbar/m $v$ in $\mathrm{m} / \mathrm{s}$ | $\begin{aligned} & 0.27 \\ & 0.09 \end{aligned}$ | $\begin{aligned} & 0.10 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.04 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.02 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 0.02 | 0.07 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 0.82 \\ 0.19 \end{array}$ | $\begin{array}{r} 0.30 \\ 0.12 \end{array}$ | $\begin{aligned} & 0.11 \\ & 0.08 \end{aligned}$ | $\begin{aligned} & 0.03 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.03 \end{aligned}$ |  |  |  |  |  |  |  |  |  |
| 0.03 | 0.11 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | 1.58 0.28 | $\begin{array}{r} 0.58 \\ 0.18 \end{array}$ | $\begin{gathered} 0.21 \\ 0.12 \end{gathered}$ | $\begin{aligned} & 0.06 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.05 \end{aligned}$ |  |  |  |  |  |  |  |  |  |
| 0.04 | 0.14 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | 2.55 0.38 | 0.93 <br> 0.25 | 0.33 0.16 | 0.10 0.09 | $\begin{aligned} & 0.04 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |  |  |  |  |  |  |
| 0.05 | 0.18 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | 3.70 0.47 | 1.34 0.31 | 0.47 0.20 | 0.15 0.12 | $\begin{aligned} & 0.05 \\ & 0.08 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.05 \end{aligned}$ |  |  |  |  |  |  |  |  |
| 0.06 | 0.22 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | 5.03 0.57 | 1.82 0.37 | 0.64 0.24 | 0.20 0.14 | $\begin{aligned} & 0.07 \\ & 0.09 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.03 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |  |  |  |  |  |
| 0.07 | 0.25 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | 6.54 0.66 | 2.36 0.43 | 0.83 <br> 0.28 <br> 1.04 | $\begin{array}{r} 0.25 \\ 0.17 \end{array}$ | $\begin{array}{r} 0.09 \\ 0.11 \\ \hline \end{array}$ | $\begin{aligned} & 0.03 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |  |  |  |  |  |
| 0.08 | 0.29 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{aligned} & 8.21 \\ & 0.76 \end{aligned}$ | 2.96 0.49 | $\begin{aligned} & 1.04 \\ & 0.31 \end{aligned}$ | $\begin{gathered} 0.32 \\ 0.19 \end{gathered}$ | $\begin{aligned} & 0.11 \\ & 0.12 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.08 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ |  |  |  |  |  |  |  |
| 0.09 | 0.32 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 10.05 \\ 0.85 \end{array}$ | $\begin{aligned} & 3.61 \\ & 0.55 \end{aligned}$ | 1.26 0.35 | $\begin{aligned} & 0.38 \\ & 0.21 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.14 \\ & 0.14 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.09 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.05 \\ & \hline \end{aligned}$ |  |  |  |  |  |  |  |
| 0.10 | 0.36 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 12.05 \\ 0.95 \end{array}$ | $\begin{aligned} & 4.32 \\ & 0.61 \end{aligned}$ | 1.51 0.39 | $\begin{aligned} & 0.46 \\ & 0.24 \end{aligned}$ | $\begin{aligned} & 0.16 \\ & 0.15 \end{aligned}$ | $\begin{array}{r} 0.06 \\ 0.10 \end{array}$ | $\begin{aligned} & 0.02 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |  |  |  |  |
| 0.12 | 0.43 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 16.52 \\ 1.14 \\ \hline \end{array}$ | $\begin{gathered} 5.90 \\ 0.74 \end{gathered}$ | 2.05 0.47 | 0.62 <br> 0.28 <br> 0.81 | $\begin{array}{r} 0.22 \\ 0.18 \\ \hline \end{array}$ | $\begin{aligned} & 0.08 \\ & 0.12 \end{aligned}$ | $\begin{aligned} & 0.03 \\ & 0.07 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ |  |  |  |  |  |  |
| 0.14 | 0.50 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 21.62 \\ 1.32 \\ \hline \end{array}$ | $\begin{aligned} & 7.70 \\ & 0.86 \end{aligned}$ | $\begin{aligned} & 2.67 \\ & 0.55 \end{aligned}$ | $\begin{aligned} & 0.81 \\ & 0.33 \end{aligned}$ | $\begin{aligned} & 0.28 \\ & 0.21 \end{aligned}$ | $\begin{aligned} & 0.10 \\ & 0.14 \end{aligned}$ | $\begin{aligned} & 0.03 \\ & 0.08 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.06 \end{aligned}$ |  |  |  |  |  |  |
| 0.16 | 0.58 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 27.33 \\ 1.51 \\ \hline \end{array}$ | $\begin{aligned} & 9.70 \\ & 0.98 \end{aligned}$ | $\begin{aligned} & 3.36 \\ & 0.63 \end{aligned}$ | $\begin{aligned} & 1.01 \\ & 0.38 \end{aligned}$ | $\begin{aligned} & 0.35 \\ & 0.24 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.13 \\ & 0.16 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0.04 \\ 0.10 \\ \hline \end{array}$ | $\begin{aligned} & 0.02 \\ & 0.07 \end{aligned}$ |  |  |  |  |  |  |
| 0.18 | 0.65 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 33.63 \\ 1.70 \\ \hline \end{array}$ | $\begin{array}{r} 11.91 \\ 1.11 \\ \hline \end{array}$ | 4.11 0.71 | 1.24 0.43 | 0.43 0.27 | 0.15 0.17 | $\begin{array}{r} 0.05 \\ 0.11 \end{array}$ | $\begin{aligned} & 0.02 \\ & 0.08 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ |  |  |  |  |  |
| 0.20 | 0.72 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 40.52 \\ 1.89 \end{array}$ | $\begin{array}{r} 14.32 \\ 1.23 \end{array}$ | $\begin{aligned} & 4.94 \\ & 0.79 \\ & \hline \end{aligned}$ | 1.48 0.47 | $\begin{aligned} & 0.52 \\ & 0.30 \end{aligned}$ | 0.18 0.19 | $\begin{array}{r} 0.06 \\ 0.12 \end{array}$ | $\begin{aligned} & 0.03 \\ & 0.09 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.06 \\ & \hline \end{aligned}$ |  |  |  |  |  |
| 0.30 | 1.08 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 83.68 \\ 2.84 \end{array}$ | $\begin{array}{r} 29.30 \\ 1.84 \end{array}$ | $\begin{array}{r} 10.01 \\ 1.18 \end{array}$ | 2.98 0.71 | 1.03 0.45 | $\begin{aligned} & 0.36 \\ & 0.29 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.12 \\ & 0.18 \end{aligned}$ | $\begin{array}{r} 0.05 \\ 0.13 \end{array}$ | $\begin{aligned} & 0.02 \\ & 0.09 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.06 \\ & \hline \end{aligned}$ |  |  |  |  |
| 0.40 | 1.44 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 140.98 \\ 3.78 \end{array}$ | $\begin{array}{r} 49.02 \\ 2.46 \end{array}$ | $\begin{array}{r} 16.64 \\ 1.57 \end{array}$ | 4.92 0.95 | 1.70 0.61 | 0.59 0.39 | 0.20 0.24 | $\begin{array}{r} 0.09 \\ 0.17 \\ \hline \end{array}$ | $\begin{gathered} 0.04 \\ 0.12 \end{gathered}$ | $\begin{aligned} & 0.01 \\ & 0.08 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.06 \\ & \hline \end{aligned}$ |  |  |  |
| 0.50 | 1.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 212.17 \\ 4.73 \end{array}$ | $\begin{array}{r} 73.35 \\ 3.07 \end{array}$ | $\begin{array}{r} 24.77 \\ 1.96 \end{array}$ | 7.29 1.18 | 2.50 0.76 | 0.87 0.49 | 0.29 0.30 | $\begin{aligned} & 0.13 \\ & 0.22 \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.15 \end{aligned}$ | $\begin{array}{r} 0.02 \\ 0.10 \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.08 \end{aligned}$ |  |  |  |
| 0.60 | 2.16 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 297.12 \\ 5.68 \end{array}$ | $\begin{array}{r} 102.21 \\ 3.68 \end{array}$ | $\begin{array}{r} 34.36 \\ 2.36 \end{array}$ | $\begin{array}{r} 10.06 \\ 1.42 \end{array}$ | 3.45 0.91 | 1.20 0.58 | 0.39 0.36 | $\begin{aligned} & 0.17 \\ & 0.26 \end{aligned}$ | $\begin{aligned} & 0.07 \\ & 0.18 \end{aligned}$ | $\begin{aligned} & 0.03 \\ & 0.12 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.09 \\ & \hline \end{aligned}$ |  |  |  |
| 0.70 | 2.52 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 395.72 \\ 6.62 \end{array}$ | $\begin{array}{r} 135.57 \\ 4.30 \end{array}$ | $\begin{array}{r} 45.40 \\ 2.75 \end{array}$ | $\begin{array}{r} 13.24 \\ 1.66 \end{array}$ | 4.52 1.06 | 1.57 0.68 | 0.51 0.42 | 0.23 0.30 | $\begin{aligned} & 0.09 \\ & 0.21 \end{aligned}$ | $\begin{array}{r} 0.04 \\ 0.14 \end{array}$ | $\begin{gathered} 0.02 \\ 0.11 \end{gathered}$ | $\begin{aligned} & 0.01 \\ & 0.07 \end{aligned}$ |  |  |
| 0.80 | 2.88 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 507.93 \\ 7.57 \\ \hline \end{array}$ | $\begin{array}{r} 173.38 \\ 4.91 \end{array}$ | $\begin{array}{r} 57.86 \\ 3.14 \end{array}$ | $\begin{array}{r} 16.82 \\ 1.89 \end{array}$ | $\begin{aligned} & 5.73 \\ & 1.21 \end{aligned}$ | $\begin{aligned} & 1.98 \\ & 0.78 \end{aligned}$ | $\begin{aligned} & 0.64 \\ & 0.49 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.28 \\ & 0.34 \end{aligned}$ | $\begin{aligned} & 0.12 \\ & 0.24 \end{aligned}$ | $\begin{aligned} & 0.05 \\ & 0.16 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0.03 \\ 0.12 \\ \hline \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.07 \end{aligned}$ |  |  |
| 0.90 | 3.24 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 633.70 \\ 8.52 \end{array}$ | $\begin{array}{r} 215.63 \\ 5.53 \\ \hline \end{array}$ | $\begin{array}{r} 71.73 \\ 3.54 \end{array}$ | $\begin{array}{r} 20.78 \\ 2.13 \\ \hline \end{array}$ | $\begin{aligned} & 7.06 \\ & 1.36 \end{aligned}$ | 2.43 0.87 | 0.79 0.55 | 0.35 0.39 | $\begin{aligned} & 0.15 \\ & 0.27 \end{aligned}$ | $\begin{array}{r} 0.06 \\ 0.18 \\ \hline \end{array}$ | $\begin{aligned} & 0.03 \\ & 0.14 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.08 \end{aligned}$ |  |  |
| 1.00 | 3.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 773.00 \\ 9.46 \end{array}$ | $\begin{array}{r} 262.30 \\ 6.14 \end{array}$ | $\begin{array}{r} 87.00 \\ 3.93 \end{array}$ | $\begin{array}{r} 25.14 \\ 2.37 \end{array}$ | $\begin{aligned} & 8.52 \\ & 1.51 \end{aligned}$ | 2.93 0.97 | 0.95 0.61 | 0.42 0.43 | $\begin{aligned} & 0.17 \\ & 0.30 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.07 \\ & 0.20 \end{aligned}$ | $\begin{array}{r} 0.04 \\ 0.15 \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.09 \end{aligned}$ |  |  |
| 1.10 | 3.96 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 925.81 \\ 10.41 \end{array}$ | $\begin{array}{r} 313.36 \\ 6.75 \end{array}$ | $\begin{array}{r} 103.67 \\ 4.32 \end{array}$ | $\begin{array}{r} 29.87 \\ 2.60 \end{array}$ | $\begin{array}{r} 10.11 \\ 1.67 \end{array}$ | 3.47 1.07 | 1.12 0.67 | 0.49 0.47 | $\begin{aligned} & 0.21 \\ & 0.33 \end{aligned}$ | 0.08 0.22 | $\begin{gathered} 0.04 \\ 0.17 \\ \hline \end{gathered}$ | $\begin{aligned} & 0.01 \\ & 0.10 \\ & \hline \end{aligned}$ |  |  |
| 1.20 | 4.32 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  | $\begin{array}{r} 368.81 \\ 7.37 \\ \hline \end{array}$ | $\begin{array}{r} 121.73 \\ 4.72 \\ \hline \end{array}$ | 34.99 2.84 | $\begin{array}{r} 11.82 \\ 1.82 \end{array}$ | 4.05 1.17 | 1.31 0.73 | 0.58 0.52 | 0.24 0.36 | 0.09 0.24 | 0.05 0.19 | 0.02 0.11 | $\begin{aligned} & 0.01 \\ & 0.07 \end{aligned}$ |  |
| 1.30 | 4.68 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  | $\begin{array}{r} 428.65 \\ 7.98 \\ \hline \end{array}$ | $\begin{array}{r} 141.17 \\ 5.11 \end{array}$ | $\begin{array}{r} 40.48 \\ 3.08 \end{array}$ | $\begin{array}{r} 13.65 \\ 1.97 \\ \hline \end{array}$ | $\begin{aligned} & 4.67 \\ & 1.26 \end{aligned}$ | 1.51 0.79 | $\begin{aligned} & 0.66 \\ & 0.56 \end{aligned}$ | $\begin{aligned} & 0.28 \\ & 0.39 \end{aligned}$ | 0.11 0.26 | $\begin{aligned} & 0.06 \\ & 0.20 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.12 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.08 \end{aligned}$ |  |
| 1.40 | 5.04 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  | $\begin{array}{r} 492.86 \\ 8.60 \end{array}$ | $\begin{array}{r} 162.00 \\ 5.50 \\ \hline \end{array}$ | $\begin{array}{r} 46.35 \\ 3.31 \\ \hline \end{array}$ | $\begin{array}{r} 15.60 \\ 2.12 \\ \hline \end{array}$ | 5.33 1.36 | $\begin{aligned} & 1.72 \\ & 0.85 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.76 \\ & 0.60 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.31 \\ & 0.42 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.12 \\ & 0.28 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.07 \\ & 0.22 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0.02 \\ 0.13 \\ \hline \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.08 \\ & \hline \end{aligned}$ |  |
| 1.60 | 5.76 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  | $\begin{array}{r} 634.39 \\ 9.82 \\ \hline \end{array}$ | $\begin{array}{r} 207.77 \\ 6.29 \\ \hline \end{array}$ | $\begin{array}{r} 59.21 \\ 3.78 \end{array}$ | $\begin{array}{r} 19.86 \\ 2.42 \\ \hline \end{array}$ | $\begin{aligned} & 6.77 \\ & 1.55 \end{aligned}$ | $\begin{aligned} & 2.18 \\ & 0.97 \end{aligned}$ | $\begin{aligned} & 0.96 \\ & 0.69 \end{aligned}$ | $\begin{aligned} & 0.40 \\ & 0.48 \end{aligned}$ | $\begin{aligned} & 0.15 \\ & 0.32 \end{aligned}$ | $\begin{aligned} & 0.08 \\ & 0.25 \end{aligned}$ | $\begin{array}{r} 0.03 \\ 0.15 \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.10 \end{aligned}$ |  |
| 1.80 | 6.48 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  | $\begin{array}{r} 793.36 \\ 11.05 \end{array}$ | $\begin{array}{r} 259.03 \\ 7.07 \\ \hline \end{array}$ | $\begin{array}{r} 73.57 \\ 4.26 \end{array}$ | $\begin{array}{r} 24.61 \\ 2.73 \end{array}$ | $\begin{aligned} & 8.37 \\ & 1.75 \\ & \hline \end{aligned}$ | 2.69 <br> 1.09 <br> 3.24 | $\begin{aligned} & 1.18 \\ & 0.77 \\ & \hline \end{aligned}$ | 0.49 <br> 0.54 <br> 0.59 | 0.19 0.36 | 0.10 0.28 | $\begin{array}{r} 0.03 \\ 0.17 \\ \hline \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.11 \\ & \hline \end{aligned}$ |  |
| 2.00 | 7.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  | $\begin{array}{r} 315.77 \\ 7.86 \end{array}$ | $\begin{array}{r} 89.40 \\ 4.73 \end{array}$ | $\begin{array}{r} 29.83 \\ 3.03 \\ \hline \end{array}$ | $\begin{array}{r} 10.12 \\ 1.94 \\ \hline \end{array}$ | $\begin{aligned} & 3.24 \\ & 1.21 \end{aligned}$ | 1.42 <br> 0.86 | 0.59 0.60 | 0.23 0.40 | 0.12 0.31 | $\begin{array}{r} 0.04 \\ 0.19 \\ \hline \end{array}$ | $\begin{gathered} 0.01 \\ 0.12 \end{gathered}$ |  |
| 2.20 | 7.92 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  | $\begin{array}{r} 377.96 \\ 8.65 \\ \hline \end{array}$ | $\begin{array}{r} 106.70 \\ 5.20 \end{array}$ | $\begin{array}{r} 35.52 \\ 3.33 \\ \hline \end{array}$ | $\begin{array}{r} 12.02 \\ 2.14 \end{array}$ | 3.85 1.34 | 1.68 0.95 | 0.69 0.65 | 0.27 0.44 | 0.14 0.34 | 0.04 0.21 | 0.02 0.13 | $\begin{aligned} & 0.01 \\ & 0.08 \end{aligned}$ |
| 2.40 | 8.64 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  | $\begin{array}{r} 445.60 \\ 9.43 \end{array}$ | $\begin{array}{r} 125.47 \\ 5.68 \end{array}$ | $\begin{array}{r} 41.67 \\ 3.63 \end{array}$ | $\begin{array}{r} 14.08 \\ 2.33 \end{array}$ | $\begin{aligned} & 4.50 \\ & 1.46 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.96 \\ & 1.03 \end{aligned}$ | $\begin{aligned} & 0.81 \\ & 0.71 \end{aligned}$ | $\begin{aligned} & 0.31 \\ & 0.48 \end{aligned}$ | 0.17 0.37 | 0.05 0.22 | 0.02 0.14 | $\begin{aligned} & 0.01 \\ & 0.09 \end{aligned}$ |
| 2.60 | 9.36 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  | $\begin{array}{r} 518.69 \\ 10.22 \end{array}$ | $\begin{array}{r} 145.71 \\ 6.15 \end{array}$ | $\begin{array}{r} 48.30 \\ 3.94 \end{array}$ | $\begin{array}{r} 16.29 \\ 2.53 \end{array}$ | $\begin{aligned} & 5.19 \\ & 1.58 \end{aligned}$ | $\begin{array}{r} 2.26 \\ 1.12 \end{array}$ | $\begin{aligned} & 0.93 \\ & 0.77 \end{aligned}$ | $\begin{aligned} & 0.36 \\ & 0.52 \end{aligned}$ | $\begin{aligned} & 0.19 \\ & 0.40 \end{aligned}$ | $\begin{aligned} & 0.06 \\ & 0.24 \end{aligned}$ | $\begin{array}{r} 0.02 \\ 0.16 \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.10 \end{aligned}$ |

## PLANNING AND DESIGN



## PLANNING AND DESIGN

|  |  | Dimension | 16 mm | 20 mm | 25 mm | 32 mm | 40 mm | 50 mm | 63 mm | 75 mm | 90 mm | 110 mm | 25 mm | 60 mm | 200 mm | m |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Wall thickness | 2.2 mm | 2.8 mm | 3.5 mm | 4.4 mm | 5.5 mm | 6.9 mm | 8.6 mm | 10.3 mm | 12.3 mm | 15.1 mm | 17.1 mm | 21.6 mm | 27.4 mm | 34.2 mm |
| 1/s | m³/h |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27.00 | 97.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 68.31 \\ 8.04 \end{array}$ | $\begin{array}{r} 25.34 \\ 5.40 \end{array}$ | $\begin{array}{r} 13.37 \\ 4.17 \end{array}$ | $\begin{aligned} & 3.88 \\ & 2.52 \end{aligned}$ | $\begin{aligned} & 1.34 \\ & 1.63 \end{aligned}$ | $\begin{aligned} & 0.45 \\ & 1.04 \end{aligned}$ |
| 28.00 | 100.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 73.20 \\ 8.34 \end{array}$ | $\begin{array}{r} 27.13 \\ 5.60 \\ \hline \end{array}$ | $\begin{array}{r} 14.31 \\ 4.32 \end{array}$ | $\begin{aligned} & 4.15 \\ & 2.61 \end{aligned}$ | 1.43 1.69 | $\begin{aligned} & 0.48 \\ & 1.08 \end{aligned}$ |
| 29.00 | 104.40 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 78.26 \\ 8.63 \end{array}$ | $\begin{array}{r} 28.98 \\ 5.80 \end{array}$ | $\begin{array}{r} 15.28 \\ 4.48 \end{array}$ | $\begin{aligned} & 4.42 \\ & 2.71 \end{aligned}$ | $\begin{aligned} & 1.53 \\ & 1.75 \end{aligned}$ | $\begin{aligned} & 0.52 \\ & 1.12 \end{aligned}$ |
| 30.00 | 108.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 83.48 \\ 8.93 \end{array}$ | $\begin{array}{r} 30.90 \\ 6.00 \end{array}$ | $\begin{array}{r} 16.28 \\ 4.63 \end{array}$ | $\begin{aligned} & 4.71 \\ & 2.80 \end{aligned}$ | 1.63 1.81 | $\begin{aligned} & 0.55 \\ & 1.16 \end{aligned}$ |
| 32.00 | 115.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 94.42 \\ 9.53 \end{array}$ | $\begin{array}{r} 34.90 \\ 6.40 \end{array}$ | $\begin{array}{r} 18.37 \\ 4.94 \end{array}$ | $\begin{aligned} & 5.31 \\ & 2.99 \end{aligned}$ | 1.83 1.93 | $\begin{aligned} & 0.62 \\ & 1.24 \end{aligned}$ |
| 34.00 | 122.40 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 106.01 \\ 10.12 \end{array}$ | $\begin{array}{r} 39.14 \\ 6.80 \end{array}$ | $\begin{array}{r} 20.59 \\ 5.25 \end{array}$ | $\begin{gathered} 5.94 \\ 3.17 \end{gathered}$ | $\begin{aligned} & 2.05 \\ & 2.05 \end{aligned}$ | $\begin{aligned} & 0.69 \\ & 1.31 \end{aligned}$ |
| 36.00 | 129.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 43.61 \\ 7.20 \end{array}$ | $\begin{array}{r} 22.93 \\ 5.56 \end{array}$ | $\begin{aligned} & 6.60 \\ & 3.36 \end{aligned}$ | $\begin{aligned} & 2.27 \\ & 2.17 \end{aligned}$ | $\begin{aligned} & 0.76 \\ & 1.39 \end{aligned}$ |
| 38.00 | 136.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 48.32 \\ 7.60 \end{array}$ | $\begin{array}{r} 25.38 \\ 5.87 \end{array}$ | $\begin{aligned} & 7.30 \\ & 3.55 \end{aligned}$ | $\begin{aligned} & 2.51 \\ & 2.29 \end{aligned}$ | $\begin{aligned} & 0.84 \\ & 1.47 \end{aligned}$ |
| 40.00 | 144.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 53.27 \\ 8.00 \end{array}$ | $\begin{array}{r} 27.96 \\ 6.18 \end{array}$ | $\begin{aligned} & 8.03 \\ & 3.73 \end{aligned}$ | $\begin{aligned} & 2.76 \\ & 2.42 \end{aligned}$ | $\begin{aligned} & 0.93 \\ & 1.54 \end{aligned}$ |
| 42.00 | 151.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 58.45 \\ 8.40 \end{array}$ | $\begin{array}{r} 30.67 \\ 6.49 \end{array}$ | $\begin{aligned} & 8.80 \\ & 3.92 \end{aligned}$ | $\begin{aligned} & 3.02 \\ & 2.54 \end{aligned}$ | $\begin{aligned} & 1.01 \\ & 1.62 \end{aligned}$ |
| 44.00 | 158.40 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 63.87 \\ 8.80 \end{array}$ | $\begin{array}{r} 33.49 \\ 6.80 \end{array}$ | $\begin{aligned} & 9.60 \\ & 4.11 \end{aligned}$ | $\begin{aligned} & 3.29 \\ & 2.66 \end{aligned}$ | $\begin{aligned} & 1.10 \\ & 1.70 \end{aligned}$ |
| 46.00 | 165.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 69.53 \\ 9.20 \end{array}$ | $\begin{array}{r} 36.43 \\ 7.10 \end{array}$ | $\begin{array}{r} 10.43 \\ 4.29 \end{array}$ | $\begin{aligned} & 3.57 \\ & 2.78 \end{aligned}$ | $\begin{aligned} & 1.20 \\ & 1.78 \end{aligned}$ |
| 48.00 | 172.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 75.42 \\ 9.60 \end{array}$ | $\begin{array}{r} 39.50 \\ 7.41 \end{array}$ | $\begin{array}{r} 11.30 \\ 4.48 \end{array}$ | $\begin{aligned} & 3.86 \\ & 2.90 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.29 \\ & 1.85 \end{aligned}$ |
| 50.00 | 180.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{aligned} & 81.54 \\ & 10.00 \end{aligned}$ | $\begin{array}{r} 42.68 \\ 7.72 \\ \hline \end{array}$ | $\begin{array}{r} 12.19 \\ 4.67 \end{array}$ | $\begin{aligned} & 4.17 \\ & 3.02 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.39 \\ & 1.93 \end{aligned}$ |
| 52.00 | 187.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 45.99 \\ 8.03 \\ \hline \end{array}$ | $\begin{array}{r} 13.13 \\ 4.85 \\ \hline \end{array}$ | $\begin{aligned} & 4.48 \\ & 3.14 \end{aligned}$ | $\begin{aligned} & 1.50 \\ & 2.01 \end{aligned}$ |
| 54.00 | 194.40 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 49.41 \\ 8.34 \end{array}$ | $\begin{array}{r} 14.09 \\ 5.04 \end{array}$ | $\begin{aligned} & 4.81 \\ & 3.26 \end{aligned}$ | $\begin{aligned} & 1.61 \\ & 2.08 \\ & \hline \end{aligned}$ |
| 56.00 | 201.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 52.96 \\ 8.65 \end{array}$ | $\begin{array}{r} 15.09 \\ 5.23 \end{array}$ | $\begin{aligned} & 5.15 \\ & 3.38 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.72 \\ & 2.16 \end{aligned}$ |
| 58.00 | 208.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 56.63 \\ 8.96 \end{array}$ | $\begin{array}{r} 16.12 \\ 5.41 \end{array}$ | $\begin{aligned} & 5.49 \\ & 3.50 \end{aligned}$ | $\begin{aligned} & 1.83 \\ & 2.24 \end{aligned}$ |
| 60.00 | 216.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 60.41 \\ 9.27 \end{array}$ | $\begin{array}{r} 17.18 \\ 5.60 \\ \hline \end{array}$ | $\begin{aligned} & 5.85 \\ & 3.62 \end{aligned}$ | $\begin{aligned} & 1.95 \\ & 2.32 \\ & \hline \end{aligned}$ |
| 62.00 | 223.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 64.32 \\ 9.57 \end{array}$ | $\begin{array}{r} 18.28 \\ 5.79 \\ \hline \end{array}$ | $\begin{array}{r} 6.22 \\ 3.74 \\ \hline \end{array}$ | $\begin{aligned} & 2.07 \\ & 2.39 \end{aligned}$ |
| 64.00 | 230.40 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 68.35 \\ 9.88 \end{array}$ | $\begin{array}{r} 19.41 \\ 5.97 \end{array}$ | $\begin{aligned} & 6.60 \\ & 3.87 \end{aligned}$ | $\begin{aligned} & 2.20 \\ & 2.47 \end{aligned}$ |
| 66.00 | 237.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & 72.50 \\ & 10.19 \end{aligned}$ | $\begin{array}{r} 20.57 \\ 6.16 \end{array}$ | $\begin{aligned} & 6.99 \\ & 3.99 \end{aligned}$ | $\begin{aligned} & 2.33 \\ & 2.55 \end{aligned}$ |
| 68.00 | 244.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 21.77 \\ 6.35 \end{array}$ | 7.39 4.11 | $\begin{aligned} & 2.46 \\ & 2.63 \end{aligned}$ |
| 70.00 | 252.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 22.99 \\ 6.53 \\ \hline \end{array}$ | $\begin{aligned} & 7.81 \\ & 4.23 \end{aligned}$ | $\begin{aligned} & 2.60 \\ & 2.70 \\ & \hline \end{aligned}$ |
| 72.00 | 259.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 24.26 \\ 6.72 \end{array}$ | 8.23 4.35 | $\begin{aligned} & 2.73 \\ & 2.78 \end{aligned}$ |
| 74.00 | 266.40 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 25.55 \\ 6.91 \end{array}$ | $\begin{aligned} & 8.66 \\ & 4.47 \end{aligned}$ | $\begin{aligned} & 2.88 \\ & 2.86 \end{aligned}$ |
| 78.00 | 280.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 28.24 \\ 7.28 \end{array}$ | $\begin{aligned} & 9.56 \\ & 4.71 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.17 \\ & 3.01 \end{aligned}$ |
| 80.00 | 288.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 29.63 \\ 7.47 \\ \hline \end{array}$ | $\begin{array}{r} 10.03 \\ 4.83 \\ \hline \end{array}$ | $\begin{aligned} & 3.33 \\ & 3.09 \end{aligned}$ |
| 82.00 | 295.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 31.05 \\ 7.65 \end{array}$ | $\begin{array}{r} 10.51 \\ 4.95 \\ \hline \end{array}$ | $\begin{aligned} & 3.48 \\ & 3.17 \end{aligned}$ |
| 84.00 | 302.40 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 32.51 \\ 7.84 \\ \hline \end{array}$ | $\begin{array}{r} 11.00 \\ 5.07 \\ \hline \end{array}$ | $\begin{aligned} & 3.64 \\ & 3.24 \\ & \hline \end{aligned}$ |
| 86.00 | 309.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 34.00 \\ 8.03 \end{array}$ | $\begin{array}{r} 11.49 \\ 5.19 \end{array}$ | $\begin{aligned} & 3.81 \\ & 3.32 \end{aligned}$ |
| 88.00 | 316.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 35.52 \\ 8.21 \end{array}$ | $\begin{array}{r} 12.00 \\ 5.31 \\ \hline \end{array}$ | $\begin{aligned} & 3.97 \\ & 3.40 \end{aligned}$ |
| 90.00 | 324.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 37.08 \\ 8.40 \end{array}$ | $\begin{array}{r} 12.52 \\ 5.44 \end{array}$ | $\begin{aligned} & 4.14 \\ & 3.47 \end{aligned}$ |

## PLANNING AND DESIGN

QUALITY
MANAGEMENT

Pressure loss due to pipe resistance R and flow rate v depending on flow V

Pipes SDR 11
Temperatur $20^{\circ} \mathrm{C} \quad$ Roughness： $0.007 \mathrm{~mm} \quad$ Density： $998.29 \mathrm{~kg} / \mathrm{m}^{3} \quad$ Kin．viscosity： $1.004 \mathrm{E}-06 \mathrm{~m}^{2} / \mathrm{s}$

|  |  | Dimension | 20 mm | 25 mm | 32 mm | 40 mm | 50 mm | 63 mm | 75 mm | 90 mm | 110 mm | 125 mm | 160 mm | 200 mm | 250 mm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Wall thickness | 1.9 mm | 2.3 mm | 2.9 mm | 3.7 mm | 4.6 mm | 5.8 mm | 6.8 mm | 8.2 mm | 10.0 mm | 11.4 mm | 14.6 mm | 18.2 mm | 22.7 mm |
| 1／s | $\mathrm{m}^{3} / \mathrm{h}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0.01 | 0.04 | R in mbar／m $v$ in $\mathrm{m} / \mathrm{s}$ | $\begin{aligned} & 0.06 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.03 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.02 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 0.02 | 0.07 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 0.18 \\ & 0.10 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.06 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.04 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.02 \\ & \hline \end{aligned}$ |  |  |  |  |  |  |  |  |  |
| 0.03 | 0.11 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 0.34 \\ 0.15 \\ \hline \end{array}$ | $\begin{aligned} & 0.12 \\ & 0.09 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.04 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |  |  |  |  |  |  |  |
| 0.04 | 0.14 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 0.54 \\ 0.19 \\ \hline \end{array}$ | 0.18 0.12 | 0.06 0.07 | 0.02 0.05 | $\begin{aligned} & 0.01 \\ & 0.03 \end{aligned}$ |  |  |  |  |  |  |  |  |
| 0.05 | 0.18 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 0.78 \\ & 0.24 \end{aligned}$ | $\begin{array}{r} 0.27 \\ 0.15 \end{array}$ | 0.08 0.09 | $\begin{aligned} & 0.03 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |  |  |  |  |  |  |
| 0.06 | 0.22 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{aligned} & 1.05 \\ & 0.29 \end{aligned}$ | 0.36 0.18 | 0.11 0.11 | $\begin{aligned} & 0.04 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.03 \end{aligned}$ |  |  |  |  |  |  |  |
| 0.07 | 0.25 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{aligned} & 1.36 \\ & 0.34 \end{aligned}$ | 0.46 0.21 | 0.14 0.13 | 0.05 0.08 | 0.02 0.05 | $\begin{aligned} & 0.01 \\ & 0.03 \end{aligned}$ |  |  |  |  |  |  |  |
| 0.08 | 0.29 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 1.70 \\ & 0.39 \end{aligned}$ | 0.58 0.24 | 0.18 0.15 | 0.06 0.10 | 0.02 0.06 | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |  |  |  |  |  |
| 0.09 | 0.32 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 2.07 \\ & 0.44 \end{aligned}$ | $\begin{aligned} & 0.70 \\ & 0.28 \end{aligned}$ | $\begin{array}{r} 0.22 \\ 0.17 \end{array}$ | $\begin{array}{r} 0.08 \\ 0.11 \\ \hline \end{array}$ | $\begin{aligned} & 0.03 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ |  |  |  |  |  |  |  |
| 0.10 | 0.36 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | 2.48 0.49 | $\begin{aligned} & 0.84 \\ & 0.31 \end{aligned}$ | 0.26 0.19 | 0.09 0.12 | 0.03 0.08 | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.03 \end{aligned}$ |  |  |  |  |  |  |
| 0.12 | 0.43 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 3.38 \\ & 0.58 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.14 \\ & 0.37 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.35 \\ & 0.22 \end{aligned}$ | 0.13 0.14 | $\begin{aligned} & 0.04 \\ & 0.09 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.02 \\ & 0.06 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \\ & \hline \end{aligned}$ |  |  |  |  |  |  |
| 0.14 | 0.50 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 4.40 \\ & 0.68 \end{aligned}$ | 1.48 0.43 | 0.46 0.26 | 0.16 0.17 | 0.06 0.11 | $\begin{aligned} & 0.02 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ |  |  |  |  |  |  |
| 0.16 | 0.58 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 5.54 \\ & 0.78 \end{aligned}$ | $\begin{aligned} & 1.86 \\ & 0.49 \end{aligned}$ | $\begin{aligned} & 0.57 \\ & 0.30 \end{aligned}$ | $\begin{array}{r} 0.20 \\ 0.19 \\ \hline \end{array}$ | $\begin{array}{r} 0.07 \\ 0.12 \\ \hline \end{array}$ | $\begin{aligned} & 0.02 \\ & 0.08 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ |  |  |  |  |  |  |
| 0.18 | 0.65 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 6.79 \\ & 0.87 \end{aligned}$ | 2.27 0.55 | 0.70 0.33 | 0.25 0.22 | 0.09 0.14 | 0.03 0.09 | $\begin{aligned} & 0.01 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.04 \\ & \hline \end{aligned}$ |  |  |  |  |  |
| 0.20 | 0.72 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{aligned} & 8.16 \\ & 0.97 \end{aligned}$ | 2.72 0.61 | 0.83 0.37 | 0.30 0.24 | 0.10 0.15 | 0.04 0.10 | $\begin{aligned} & 0.02 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ |  |  |  |  |  |
| 0.30 | 1.08 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 16.61 \\ 1.46 \end{array}$ | $\begin{aligned} & 5.50 \\ & 0.92 \end{aligned}$ | $\begin{aligned} & 1.67 \\ & 0.56 \end{aligned}$ | 0.59 0.36 | $\begin{aligned} & 0.21 \\ & 0.23 \end{aligned}$ | 0.07 0.14 | 0.03 0.10 | $\begin{aligned} & 0.01 \\ & 0.07 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.05 \end{aligned}$ |  |  |  |  |
| 0.40 | 1.44 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 27.68 \\ 1.94 \end{array}$ | $\begin{aligned} & 9.11 \\ & 1.22 \end{aligned}$ | 2.75 0.74 | 0.97 0.48 | 0.34 0.31 | 0.11 0.19 | 0.05 0.14 | $\begin{aligned} & 0.02 \\ & 0.09 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.06 \end{aligned}$ |  |  |  |  |
| 0.50 | 1.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 41.30 \\ 2.43 \end{array}$ | $\begin{array}{r} 13.53 \\ 1.53 \\ \hline \end{array}$ | $\begin{aligned} & 4.07 \\ & 0.93 \end{aligned}$ | $\begin{aligned} & 1.43 \\ & 0.60 \end{aligned}$ | 0.49 0.38 | $\begin{aligned} & 0.17 \\ & 0.24 \\ & \hline \end{aligned}$ | $\begin{gathered} 0.07 \\ 0.17 \\ \hline \end{gathered}$ | $\begin{array}{r} 0.03 \\ 0.12 \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.08 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.06 \end{aligned}$ |  |  |  |
| 0.60 | 2.16 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 57.42 \\ 2.91 \\ \hline \end{array}$ | $\begin{array}{r} 18.73 \\ 1.84 \\ \hline \end{array}$ | $\begin{array}{r} 5.61 \\ 1.11 \\ \hline \end{array}$ | $\begin{aligned} & 1.97 \\ & 0.72 \end{aligned}$ | 0.68 0.46 | $\begin{aligned} & 0.23 \\ & 0.29 \end{aligned}$ | $\begin{aligned} & 0.10 \\ & 0.20 \end{aligned}$ | $\begin{gathered} 0.04 \\ 0.14 \end{gathered}$ | $\begin{aligned} & 0.02 \\ & 0.09 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.07 \end{aligned}$ |  |  |  |
| 0.70 | 2.52 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 75.99 \\ 3.40 \\ \hline \end{array}$ | $\begin{array}{r} 24.69 \\ 2.14 \\ \hline \end{array}$ | $\begin{aligned} & 7.37 \\ & 1.30 \end{aligned}$ | 2.58 0.84 | 0.89 0.54 | 0.30 0.34 | 0.13 0.24 | $\begin{aligned} & 0.05 \\ & 0.16 \\ & \hline \end{aligned}$ | $\begin{gathered} 0.02 \\ 0.11 \end{gathered}$ | $\begin{aligned} & 0.01 \\ & 0.09 \\ & \hline \end{aligned}$ |  |  |  |
| 0.80 | 2.88 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 97.01 \\ 3.88 \end{array}$ | $\begin{array}{r} 31.41 \\ 2.45 \end{array}$ | $\begin{aligned} & 9.34 \\ & 1.48 \end{aligned}$ | 3.27 0.96 | 1.12 0.61 | 0.37 0.39 | 0.16 0.27 | $\begin{aligned} & 0.07 \\ & 0.19 \end{aligned}$ | $\begin{array}{r} 0.03 \\ 0.13 \\ \hline \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.10 \\ & \hline \end{aligned}$ |  |  |  |
| 0.90 | 3.24 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 120.44 \\ 4.37 \end{array}$ | $\begin{array}{r} 38.87 \\ 2.75 \end{array}$ | $\begin{array}{r} 11.53 \\ 1.67 \end{array}$ | 4.02 1.08 | 1.37 0.69 | 0.46 0.43 | 0.20 0.30 | $\begin{aligned} & 0.08 \\ & 0.21 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0.03 \\ 0.14 \end{array}$ | $\begin{gathered} 0.02 \\ 0.11 \end{gathered}$ | $\begin{aligned} & 0.01 \\ & 0.07 \end{aligned}$ |  |  |
| 1.00 | 3.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 146.28 \\ 4.85 \end{array}$ | $\begin{array}{r} 47.08 \\ 3.06 \end{array}$ | $\begin{array}{r} 13.93 \\ 1.85 \end{array}$ | 4.85 1.20 | 1.65 0.76 | 0.55 0.48 | 0.24 0.34 | 0.10 0.24 | $\begin{array}{r} 0.04 \\ 0.16 \end{array}$ | $\begin{array}{r} 0.02 \\ 0.12 \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.07 \end{aligned}$ |  |  |
| 1.10 | 3.96 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 174.52 \\ 5.34 \end{array}$ | $\begin{array}{r} 56.03 \\ 3.37 \end{array}$ | $\begin{array}{r} 16.53 \\ 2.04 \end{array}$ | 5.74 1.32 | 1.96 0.84 | 0.65 0.53 | 0.28 0.37 | 0.12 0.26 | 0.05 0.17 | 0.02 0.13 | $\begin{aligned} & 0.01 \\ & 0.08 \end{aligned}$ |  |  |
| 1.20 | 4.32 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 205.14 \\ 5.82 \end{array}$ | $\begin{array}{r} 65.70 \\ 3.67 \end{array}$ | $\begin{array}{r} 19.34 \\ 2.23 \end{array}$ | $\begin{aligned} & 6.71 \\ & 1.44 \\ & \hline \end{aligned}$ | 2.28 0.92 | $\begin{aligned} & 0.76 \\ & 0.58 \end{aligned}$ | $\begin{aligned} & 0.32 \\ & 0.41 \end{aligned}$ | $\begin{aligned} & 0.14 \\ & 0.28 \end{aligned}$ | 0.05 0.19 | $\begin{aligned} & 0.03 \\ & 0.15 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.09 \end{aligned}$ |  |  |
| 1.30 | 4.68 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 238.15 \\ 6.31 \end{array}$ | $\begin{array}{r} 76.11 \\ 3.98 \end{array}$ | $\begin{array}{r} 22.36 \\ 2.41 \end{array}$ | 7.74 1.56 | 2.63 0.99 | 0.87 0.63 | $\begin{aligned} & 0.37 \\ & 0.44 \end{aligned}$ | 0.16 0.31 | $\begin{aligned} & 0.06 \\ & 0.20 \end{aligned}$ | $\begin{array}{r} 0.03 \\ 0.16 \\ \hline \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.10 \end{aligned}$ |  |  |
| 1.40 | 5.04 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 273.54 \\ 6.79 \end{array}$ | $\begin{array}{r} 87.24 \\ 4.28 \\ \hline \end{array}$ | $\begin{array}{r} 25.57 \\ 2.60 \end{array}$ | $\begin{aligned} & 8.84 \\ & 1.68 \end{aligned}$ | $\begin{aligned} & 3.00 \\ & 1.07 \\ & \hline \end{aligned}$ | 0.99 0.67 | $\begin{aligned} & 0.42 \\ & 0.47 \end{aligned}$ | 0.18 0.33 | $\begin{aligned} & 0.07 \\ & 0.22 \end{aligned}$ | $\begin{gathered} 0.04 \\ 0.17 \end{gathered}$ | $\begin{aligned} & 0.01 \\ & 0.10 \end{aligned}$ |  |  |
| 1.60 | 5.76 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ | $\begin{array}{r} 351.43 \\ 7.76 \end{array}$ | $\begin{array}{r} 111.67 \\ 4.90 \end{array}$ | $\begin{array}{r} 32.61 \\ 2.97 \end{array}$ | $\begin{array}{r} 11.25 \\ 1.92 \end{array}$ | 3.80 1.22 | 1.25 0.77 | 0.54 0.54 | 0.23 0.38 | 0.09 0.25 | $\begin{aligned} & 0.05 \\ & 0.20 \end{aligned}$ | $\begin{gathered} 0.01 \\ 0.12 \end{gathered}$ |  |  |
| 1.80 | 6.48 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 438.78 \\ 8.73 \end{array}$ | $\begin{array}{r} 138.97 \\ 5.51 \\ \hline \end{array}$ | 40.45 3.34 | $\begin{array}{r} 13.91 \\ 2.16 \end{array}$ | 4.69 1.38 | 1.54 0.87 | 0.66 0.61 | 0.28 0.42 | 0.11 <br> 0.28 <br> 0. | 0.06 0.22 | 0.02 0.13 | $\begin{aligned} & 0.01 \\ & 0.09 \end{aligned}$ |  |
| 2.00 | 7.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 535.58 \\ 9.70 \end{array}$ | $\begin{array}{r} 169.14 \\ 6.12 \end{array}$ | $\begin{array}{r} 49.09 \\ 3.71 \end{array}$ | $\begin{array}{r} 16.84 \\ 2.40 \end{array}$ | $\begin{aligned} & 5.67 \\ & 1.53 \end{aligned}$ | 1.86 0.96 | $\begin{aligned} & 0.79 \\ & 0.68 \end{aligned}$ | 0.33 0.47 | 0.13 0.31 | $\begin{aligned} & 0.07 \\ & 0.24 \end{aligned}$ | $\begin{array}{r} 0.02 \\ 0.15 \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.10 \end{aligned}$ |  |
| 2.20 | 7.92 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ | $\begin{array}{r} 641.81 \\ 10.67 \end{array}$ | $\begin{array}{r} 202.17 \\ 6.73 \end{array}$ | $\begin{array}{r} 58.51 \\ 4.08 \end{array}$ | $\begin{array}{r} 20.03 \\ 2.64 \end{array}$ | $\begin{aligned} & 6.73 \\ & 1.68 \end{aligned}$ | $\begin{aligned} & 2.21 \\ & 1.06 \end{aligned}$ | $\begin{aligned} & 0.94 \\ & 0.74 \end{aligned}$ | $\begin{aligned} & 0.39 \\ & 0.52 \end{aligned}$ | $\begin{aligned} & 0.15 \\ & 0.35 \end{aligned}$ | $\begin{aligned} & 0.08 \\ & 0.27 \end{aligned}$ | $\begin{array}{r} 0.03 \\ 0.16 \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.10 \end{aligned}$ |  |
| 2.40 | 8.64 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  | $\begin{array}{r} 238.06 \\ 7.34 \\ \hline \end{array}$ | $\begin{array}{r} 68.72 \\ 4.45 \end{array}$ | $\begin{array}{r} 23.48 \\ 2.88 \end{array}$ | $\begin{aligned} & 7.87 \\ & 1.84 \end{aligned}$ | $\begin{array}{r} 2.58 \\ 1.16 \\ \hline \end{array}$ | 1.10 0.81 | $\begin{aligned} & 0.46 \\ & 0.56 \end{aligned}$ | $\begin{aligned} & 0.18 \\ & 0.38 \end{aligned}$ | $\begin{aligned} & 0.10 \\ & 0.29 \end{aligned}$ | $\begin{array}{r} 0.03 \\ 0.18 \\ \hline \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.11 \end{aligned}$ |  |
| 2.60 | 9.36 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  | $\begin{array}{r} 276.78 \\ 7.95 \\ \hline \end{array}$ | $\begin{array}{r} 79.71 \\ 4.82 \end{array}$ | $\begin{array}{r} 27.18 \\ 3.11 \end{array}$ | $\begin{aligned} & 9.10 \\ & 1.99 \end{aligned}$ | $\begin{aligned} & 2.97 \\ & 1.25 \end{aligned}$ | $\begin{aligned} & 1.26 \\ & 0.88 \end{aligned}$ | $\begin{aligned} & 0.53 \\ & 0.61 \end{aligned}$ | $\begin{aligned} & 0.20 \\ & 0.41 \end{aligned}$ | $\begin{aligned} & 0.11 \\ & 0.32 \end{aligned}$ | $\begin{array}{r} 0.03 \\ 0.19 \end{array}$ | $\begin{aligned} & 0.01 \\ & 0.12 \end{aligned}$ |  |

## PLANNING AND DESIGN



## PLANNING AND DESIGN

|  |  | Dimension | 20 mm | 25 mm | 32 mm | 40 mm | 50 mm | 63 mm | 75 mm | 90 mm | 110 mm | 125 mm | 160 mm | 200 mm | 250 mm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Wall thickness | 1.9 mm | 2.3 mm | 2.9 mm | 3.7 mm | 4.6 mm | 5.8 mm | 6.8 mm | 8.2 mm | 10.0 mm | 11.4 mm | 14.6 mm | 18.2 mm | 22.7 mm |
| 1／s | $\mathrm{m}^{3} \mathrm{~h}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27.00 | 97.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  | $\begin{array}{r} 93.72 \\ 9.12 \\ \hline \end{array}$ | $\begin{array}{r} 37.88 \\ 6.35 \\ \hline \end{array}$ | $\begin{array}{r} 13.97 \\ 4.24 \\ \hline \end{array}$ | $\begin{aligned} & 7.46 \\ & 3.29 \end{aligned}$ | $\begin{aligned} & 2.23 \\ & 2.01 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.75 \\ & 1.28 \end{aligned}$ | $\begin{aligned} & 0.25 \\ & 0.82 \end{aligned}$ |
| 28.00 | 100.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  | $\begin{array}{r} 100.46 \\ 9.46 \\ \hline \end{array}$ | $\begin{array}{r} 40.57 \\ 6.58 \\ \hline \end{array}$ | $\begin{array}{r} 14.95 \\ 4.40 \end{array}$ | $\begin{aligned} & 7.99 \\ & 3.41 \end{aligned}$ | $\begin{aligned} & 2.38 \\ & 2.08 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.80 \\ & 1.33 \end{aligned}$ | $\begin{aligned} & 0.27 \\ & 0.85 \end{aligned}$ |
| 29.00 | 104.40 | R |  |  |  |  |  |  | $\begin{array}{r} 107.42 \\ 9.79 \\ \hline \end{array}$ | $\begin{array}{r} 43.36 \\ 6.82 \\ \hline \end{array}$ | $\begin{array}{r} 15.96 \\ 4.56 \\ \hline \end{array}$ | $\begin{aligned} & 8.52 \\ & 3.54 \end{aligned}$ | $\begin{array}{r} 2.54 \\ 2.16 \\ \hline \end{array}$ | $\begin{aligned} & 0.86 \\ & 1.38 \end{aligned}$ | $\begin{aligned} & 0.29 \\ & 0.88 \end{aligned}$ |
| 30.00 | 108.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  | $\begin{array}{r} 114.61 \\ 10.13 \\ \hline \end{array}$ | $\begin{array}{r} 46.23 \\ 7.05 \\ \hline \end{array}$ | $\begin{array}{r} 17.01 \\ 4.72 \\ \hline \end{array}$ | $\begin{aligned} & 9.08 \\ & 3.66 \end{aligned}$ | $\begin{aligned} & 2.71 \\ & 2.23 \end{aligned}$ | $\begin{aligned} & 0.91 \\ & 1.43 \end{aligned}$ | $\begin{aligned} & 0.31 \\ & 0.91 \end{aligned}$ |
| 32.00 | 115.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  | $\begin{array}{r} 52.25 \\ 7.52 \\ \hline \end{array}$ | $\begin{array}{r} 19.20 \\ 5.03 \\ \hline \end{array}$ | $\begin{array}{r} 10.24 \\ 3.90 \\ \hline \end{array}$ | $\begin{aligned} & 3.05 \\ & 2.38 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.02 \\ & 1.52 \end{aligned}$ | $\begin{aligned} & 0.35 \\ & 0.97 \end{aligned}$ |
| 34.00 | 122.40 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  | $\begin{array}{r} 58.62 \\ 7.99 \\ \hline \end{array}$ | $\begin{array}{r} 21.51 \\ 5.34 \\ \hline \end{array}$ | $\begin{array}{r} 11.46 \\ 4.14 \\ \hline \end{array}$ | $\begin{aligned} & 3.41 \\ & 2.53 \end{aligned}$ | $\begin{aligned} & 1.14 \\ & 1.62 \end{aligned}$ | $\begin{aligned} & 0.39 \\ & 1.03 \end{aligned}$ |
| 36.00 | 129.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  | $\begin{array}{r} 65.36 \\ 8.46 \\ \hline \end{array}$ | $\begin{array}{r} 23.96 \\ 5.66 \\ \hline \end{array}$ | $\begin{array}{r} 12.76 \\ 4.39 \\ \hline \end{array}$ | $\begin{aligned} & 3.79 \\ & 2.68 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.27 \\ & 1.71 \end{aligned}$ | $\begin{aligned} & 0.43 \\ & 1.09 \end{aligned}$ |
| 38.00 | 136.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  | $\begin{array}{r} 72.45 \\ 8.93 \\ \hline \end{array}$ | $\begin{array}{r} 26.53 \\ 5.97 \\ \hline \end{array}$ | $\begin{array}{r} 14.12 \\ 4.63 \\ \hline \end{array}$ | $\begin{array}{r} 4.19 \\ 2.83 \end{array}$ | $\begin{aligned} & 1.40 \\ & 1.81 \end{aligned}$ | $\begin{aligned} & 0.47 \\ & 1.16 \end{aligned}$ |
| 40.00 | 144.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  | $\begin{array}{r} 79.90 \\ 9.40 \\ \hline \end{array}$ | $\begin{array}{r} 29.22 \\ 6.29 \\ \hline \end{array}$ | $\begin{array}{r} 15.54 \\ 4.88 \\ \hline \end{array}$ | $\begin{aligned} & 4.60 \\ & 2.98 \end{aligned}$ | $\begin{aligned} & 1.54 \\ & 1.90 \end{aligned}$ | 0.52 1.22 |
| 42.00 | 151.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  | $\begin{array}{r} 87.71 \\ 9.87 \end{array}$ | $\begin{array}{r} 32.05 \\ 6.60 \\ \hline \end{array}$ | $\begin{array}{r} 17.03 \\ 5.12 \\ \hline \end{array}$ | $\begin{gathered} 5.04 \\ 3.13 \end{gathered}$ | $\begin{aligned} & 1.68 \\ & 2.00 \end{aligned}$ | $\begin{aligned} & 0.57 \\ & 1.28 \end{aligned}$ |
| 44.00 | 158.40 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  | $\begin{aligned} & 95.87 \\ & 10.34 \end{aligned}$ | $\begin{array}{r} 35.00 \\ 6.92 \end{array}$ | $\begin{array}{r} 18.59 \\ 5.36 \\ \hline \end{array}$ | $\begin{aligned} & 5.49 \\ & 3.27 \end{aligned}$ | $\begin{aligned} & 1.84 \\ & 2.09 \end{aligned}$ | $\begin{aligned} & 0.62 \\ & 1.34 \end{aligned}$ |
| 46.00 | 165.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 38.08 \\ 7.23 \end{array}$ | $\begin{array}{r} 20.21 \\ 5.61 \\ \hline \end{array}$ | $\begin{array}{r} 5.97 \\ 3.42 \end{array}$ | $\begin{aligned} & 1.99 \\ & 2.19 \end{aligned}$ | 0.67 1.40 |
| 48.00 | 172.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 41.28 \\ 7.55 \\ \hline \end{array}$ | $\begin{array}{r} 21.90 \\ 5.85 \\ \hline \end{array}$ | $\begin{aligned} & 6.46 \\ & 3.57 \end{aligned}$ | $\begin{aligned} & 2.15 \\ & 2.28 \end{aligned}$ | $\begin{aligned} & 0.72 \\ & 1.46 \end{aligned}$ |
| 50.00 | 180.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 44.61 \\ 7.86 \end{array}$ | $\begin{array}{r} 23.66 \\ 6.10 \\ \hline \end{array}$ | $\begin{aligned} & 6.97 \\ & 3.72 \end{aligned}$ | $\begin{aligned} & 2.32 \\ & 2.38 \end{aligned}$ | $\begin{aligned} & 0.78 \\ & 1.52 \end{aligned}$ |
| 52.00 | 187.20 | R |  |  |  |  |  |  |  |  | $\begin{array}{r} 48.07 \\ 8.17 \\ \hline \end{array}$ | $\begin{array}{r} 25.48 \\ 6.34 \\ \hline \end{array}$ | $\begin{aligned} & 7.50 \\ & 3.87 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.50 \\ & 2.47 \\ & \hline \end{aligned}$ | 0.84 1.58 |
| 54.00 | 194.40 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 51.65 \\ 8.49 \\ \hline \end{array}$ | $\begin{array}{r} 27.37 \\ 6.58 \\ \hline \end{array}$ | $\begin{aligned} & 8.05 \\ & 4.02 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.68 \\ & 2.57 \end{aligned}$ | $\begin{aligned} & 0.90 \\ & 1.64 \end{aligned}$ |
| 56.00 | 201.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 55.36 \\ 8.80 \\ \hline \end{array}$ | $\begin{array}{r} 29.32 \\ 6.83 \\ \hline \end{array}$ | $\begin{aligned} & 8.61 \\ & 4.17 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.86 \\ & 2.66 \end{aligned}$ | $\begin{aligned} & 0.96 \\ & 1.70 \end{aligned}$ |
| 58.00 | 208.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 59.20 \\ 9.12 \\ \hline \end{array}$ | $\begin{array}{r} 31.34 \\ 7.07 \\ \hline \end{array}$ | $\begin{aligned} & 9.20 \\ & 4.32 \end{aligned}$ | $\begin{aligned} & 3.06 \\ & 2.76 \end{aligned}$ | $\begin{aligned} & 1.02 \\ & 1.76 \end{aligned}$ |
| 60.00 | 216.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 63.16 \\ 9.43 \end{array}$ | $\begin{array}{r} 33.42 \\ 7.31 \end{array}$ | $\begin{aligned} & 9.80 \\ & 4.47 \end{aligned}$ | $\begin{aligned} & 3.25 \\ & 2.85 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.09 \\ & 1.82 \end{aligned}$ |
| 62.00 | 223.20 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{array}{r} 67.24 \\ 9.75 \\ \hline \end{array}$ | $\begin{array}{r} 35.57 \\ 7.56 \end{array}$ | $\begin{array}{r} 10.42 \\ 4.61 \\ \hline \end{array}$ | $\begin{aligned} & 3.46 \\ & 2.95 \end{aligned}$ | $\begin{aligned} & 1.16 \\ & 1.89 \end{aligned}$ |
| 64.00 | 230.40 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{aligned} & 71.46 \\ & 10.06 \\ & \hline \end{aligned}$ | $\begin{array}{r} 37.78 \\ 7.80 \\ \hline \end{array}$ | $\begin{array}{r} 11.06 \\ 4.76 \\ \hline \end{array}$ | $\begin{aligned} & 3.67 \\ & 3.04 \end{aligned}$ | $\begin{aligned} & 1.23 \\ & 1.95 \end{aligned}$ |
| 66.00 | 237.60 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 40.06 \\ 8.05 \end{array}$ | $\begin{array}{r} 11.72 \\ 4.91 \\ \hline \end{array}$ | $\begin{aligned} & 3.88 \\ & 3.14 \end{aligned}$ | $\begin{aligned} & 1.30 \\ & 2.01 \end{aligned}$ |
| 68.00 | 244.80 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 42.40 \\ 8.29 \\ \hline \end{array}$ | $\begin{array}{r} 12.40 \\ 5.06 \\ \hline \end{array}$ | $\begin{aligned} & 4.11 \\ & 3.23 \end{aligned}$ | $\begin{aligned} & 1.37 \\ & 2.07 \end{aligned}$ |
| 70.00 | 252.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 44.81 \\ 8.53 \\ \hline \end{array}$ | $\begin{array}{r} 13.10 \\ 5.21 \\ \hline \end{array}$ | $\begin{aligned} & 4.33 \\ & 3.33 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.45 \\ & 2.13 \end{aligned}$ |
| 75.00 | 270.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 51.12 \\ 9.14 \end{array}$ | $\begin{array}{r} 14.91 \\ 5.58 \\ \hline \end{array}$ | $\begin{aligned} & 4.93 \\ & 3.57 \end{aligned}$ | $\begin{aligned} & 1.64 \\ & 2.28 \end{aligned}$ |
| 80.00 | 288.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 57.84 \\ 9.75 \\ \hline \end{array}$ | $\begin{array}{r} 16.85 \\ 5.95 \\ \hline \end{array}$ | $\begin{aligned} & 5.56 \\ & 3.81 \end{aligned}$ | $\begin{aligned} & 1.85 \\ & 2.43 \end{aligned}$ |
| 85.00 | 306.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{aligned} & 64.96 \\ & 10.36 \\ & \hline \end{aligned}$ | $\begin{array}{r} 18.90 \\ 6.33 \\ \hline \end{array}$ | $\begin{aligned} & 6.23 \\ & 4.04 \end{aligned}$ | $\begin{aligned} & 2.07 \\ & 2.59 \end{aligned}$ |
| 90.00 | 324.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 21.06 \\ 6.70 \\ \hline \end{array}$ | $\begin{aligned} & 6.93 \\ & 4.28 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.30 \\ & 2.74 \\ & \hline \end{aligned}$ |
| 95.00 | 342.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 23.33 \\ 7.07 \end{array}$ | $\begin{aligned} & 7.67 \\ & 4.52 \end{aligned}$ | $\begin{aligned} & 2.55 \\ & 2.89 \end{aligned}$ |
| 100.00 | 360.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 25.72 \\ 7.44 \\ \hline \end{array}$ | $\begin{aligned} & 8.45 \\ & 4.76 \end{aligned}$ | $\begin{aligned} & 2.80 \\ & 3.04 \\ & \hline \end{aligned}$ |
| 110.00 | 396.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 30.85 \\ 8.19 \\ \hline \end{array}$ | $\begin{array}{r} 10.11 \\ 5.23 \\ \hline \end{array}$ | $\begin{aligned} & 3.35 \\ & 3.35 \end{aligned}$ |
| 120.00 | 432.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 36.42 \\ 8.93 \\ \hline \end{array}$ | $\begin{array}{r} 11.92 \\ 5.71 \\ \hline \end{array}$ | $\begin{aligned} & 3.94 \\ & 3.65 \end{aligned}$ |
| 130.00 | 468.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 42.45 \\ 9.67 \end{array}$ | $\begin{array}{r} 13.87 \\ 6.18 \\ \hline \end{array}$ | $\begin{aligned} & 4.58 \\ & 3.95 \end{aligned}$ |
| 140.00 | 504.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & 48.94 \\ & 10.42 \\ & \hline \end{aligned}$ | $\begin{array}{r} 15.96 \\ 6.66 \\ \hline \end{array}$ | $\begin{aligned} & 5.26 \\ & 4.26 \end{aligned}$ |
| 150.00 | 540.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{~V} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 55.87 \\ 11.16 \\ \hline \end{array}$ | $\begin{array}{r} 18.20 \\ 7.14 \end{array}$ | $\begin{aligned} & 5.99 \\ & 4.56 \end{aligned}$ |
| 160.00 | 576.00 | $\underset{v}{R}$ |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & 63.26 \\ & 11.91 \\ & \hline \end{aligned}$ | $\begin{array}{r} 20.58 \\ 7.61 \\ \hline \end{array}$ | $\begin{aligned} & 6.76 \\ & 4.87 \end{aligned}$ |
| 170.00 | 612.00 | $\begin{aligned} & \mathrm{R} \\ & \mathrm{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & 71.10 \\ & 12.65 \\ & \hline \end{aligned}$ | $\begin{array}{r} 23.10 \\ 8.09 \end{array}$ | $\begin{aligned} & 7.58 \\ & 5.17 \end{aligned}$ |

## PLANNING AND DESIGN

## 5．2 Simplified Procedure

## General information

This section describes a simple method suitable to determine the inner pipe diameters for standard installations． The procedure can be applied to all building types，which do not have above－average dimensions．This means that the simplified procedure is suitable for the vast majority of all buildings．
The method is applied in the same way for both cold and hot water pipes．

## Differentiating calculation procedure

The planner is free to determine the inner pipe diameters through the use of nationally recognised differentiating methods of calculation．

## Hot water circulation pipes

Hot water circulation pipes are subject to other hydraulic laws and cannot be measured with this method． Flow velocities in hot water circulation pipes must be determined in accordance with national recommendations or manufacturer guidelines

## Load unit

1 load unit（LU）is equal to a tapping point fitting flow rate $Q_{A}$ of $0.1 \mathrm{l} / \mathrm{s}$ ．
Tapping point fitting flow rates $Q_{A}$ ，minimum draw－off point fitting flow rates $Q_{\text {min }}$ and load units for tapping points

| Tapping point | $\mathbf{Q}_{\mathrm{A}}$ | $\mathbf{Q}_{\min }$ | Load unit |
| :--- | :---: | :---: | :---: |
|  | $\mathrm{I} / \mathrm{s}$ | $\mathrm{I} / \mathrm{s}$ |  |
| wash basin，hand basin，bidet，cistern | 0.1 | 0.1 | 1 |
| household kitchen sink，household washing machine＊，dishwasher，utility sink，shower head | 0.2 | 0.15 | 2 |
| urinal flusher | 0.3 | 0.15 | 3 |
| bath tub outlet | 0.4 | 0.3 | 4 |
| garden／garage tap | 0.5 | 0.4 | 5 |
| commercial kitchen sink DN 20，commercial bath tub outlet | 0.8 | 0.8 | 8 |
| flusher DN 20 | 1.5 | 1.0 | 15 |

＊for commercial washing machines refer to the manufacturer＇s recommendations

The values listed above do not correspond to the values provided in product standards．They are merely used for the determination of inner pipe diameters．

## Application of the simplified procedure

Starting from the farthest tapping point，the load units for the installation＇s individual pipe sections must be determined．The load units are then added．The probability of simultaneous use and of peak flow QD has been taken into account in the table of load values．Therefore，the inner pipe diameter can be obtained from the table．

The simplified calculation procedure is based on following flow rates．

Collecting lines risers，floor level lines
maximum $2.0 \mathrm{~m} / \mathrm{s}$
Single supply lines
maximum $4.0 \mathrm{~m} / \mathrm{s}$

Note：National regulations may require lower flow rates，in order to prevent pressure surges and noise．

## PLANNING AND DESIGN

Load units LU for the determination of the inner pipe diameters
Table 13

| PP pipe SDR 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| maximum load value | LU | 1 | 2 | 3 | 3 | 4 | 6 | 13 | 30 | 70 | 200 | 540 | 970 |
| greatest single value | LU |  |  | 2 |  |  | 4 | 5 | 8 |  |  |  |  |
| $\mathrm{d}_{\mathrm{a}} \times \mathrm{S}$ | mm | $16 \times 2.7$ |  |  | $\mathbf{2 0} \times 3.4$ |  |  | $25 \times 4.2$ | $32 \times 5.4$ | $40 \times 6.7$ | $50 \times 8.4$ | $63 \times 10.5$ | $75 \times 12.5$ |
| $\mathrm{d}_{\mathrm{i}}$ | mm | 10.6 |  |  | 13.2 |  |  | 16.6 | 21.2 | 26.6 | 33.2 | 42 | 50 |
| maximum pipe length | m | 20 | 12 | 8 | 15 | 9 | 7 |  |  |  |  |  |  |

## Example: Determining the inner pipe diameter for standard installations



## PLANNING AND DESIGN

## Implementation

Starting from the farthest tapping point，the load units for the individual pipe sections must be added．Then， the inner pipe diameters are determined．

## Definition of tasks in accordance with the installation plan

Calculate the cold water pipe leading from the basement to the tapping points．Calculate the pipeline as required for plastic pipes made of PP．

The following tapping points are installed in every apartment：
1 bath tub
1 WC with cistern
1 wash basin
1 household kitchen sink
There are five similar apartments in total．

## Solution

The load units are to be determined according to
Table 13：
1 bath tub 4 LU

1 WC with cistern 1 LU
1 wash basin 1 LU
1 household kitchen sink 2 LU

## Section 1

1 kitchen sink connected $=2 \mathrm{LU}$
Table 13 shows $2 L U=$ pipe 16 mm ，
maximum length 8 m

## Section 2

| 1 kitchen sink connected | $=2 \mathrm{LU}$ |
| :--- | :--- |
| 1 bath connected | $=4 \mathrm{LU}$ |
| Total | $=6 \mathrm{LU}$ |

Table 13 shows $6 \mathrm{LU}=$ pipe 20 mm ， maximum length 7 m

## Section 3

| 1 kitchen sink connected | $=2 \mathrm{LU}$ |
| :--- | :--- |
| 1 bath connected | $=4 \mathrm{LU}$ |
| 1 wash basin connected | $=1 \mathrm{LU}$ |
| Total | $=7 \mathrm{LU}$ |

Table 13 shows $7 \mathrm{LU}=$ pipe 25 mm

## Section 4

| 1 kitchen sink | $=2 \mathrm{LU}$ |
| :--- | :--- |
| 1 bath | $=4 \mathrm{LU}$ |
| 1 wash basin | $=1 \mathrm{LU}$ |
| 1 cistern | $=1 \mathrm{LU}$ |
| Total for 1 apartment | $=8 \mathrm{LU}$ |

Table 13 shows $8 \mathrm{LU}=$ pipe 25 mm

## Section 5

2 apartments connected $=16 \mathrm{LU}$
Table 13 shows $16 \mathrm{LU}=$ pipe 32 mm

## Section 6

3 apartments connected $=24 \mathrm{LU}$
Table 13 shows $24 L U=$ pipe 32 mm
Section 7
4 apartments connected $=32 \mathrm{LU}$
Table 13 shows $32 \mathrm{LU}=$ pipe 40 mm

## Section 8

5 apartments connected $=40 \mathrm{LU}$
Table 13 shows $40 \mathrm{LU}=$ pipe 40 mm

## WELDING TECHNOLOGY

### 6.1 Basic Information

### 6.1.1 Socket Welding Using a Heated Tool

Before starting the work, make sure that the welding tools lie flat against the heated rod. Do not use pliers or other unsuitable tools for the assembly, to avoid damage to the coating of the welding tools.

The required welding temperature for processing the POLO-ECOSAN installation system is $250-270{ }^{\circ} \mathrm{C}$.

## Warning

- Danger of burns from hot welding equipment
- The first welding should not be carried out until five minutes after the welding temperature has been reached!

POLO-ECOSAN welding equipment and welding tools must be protected against impurities. Burned-on particles can lead to faulty welding connections. Tools may be cleaned with non-fibrous, coarse paper towels. The welding tools must be kept dry at all times.

Damaged and soiled welding tools must be replaced, since only impeccable processing tools can ensure impeccable connections.

Connect the components during the welding process without twisting the parts. Minor corrections can only be made immediately after the parts are connected.

### 6.1.2 Guidelines

General work protection and accident prevention guidelines are to be observed when using welding equipment.
The Guidelines of the Industrial Trade Associations of the Chemical Industry for Machines for the Processing and Employment of Plastics, Chapter: Welding Machines and Equipment, apply.

For the handling of POLO-ECOSAN welding equipment, machines and tools, the General Guidelines DVS 2208, Section 1 apply. In order to establish a connection between the POLO-ECOSAN pipe and the fitted part, the welding tools used must correspond to the measurements as stipulated by procedure A.

In accordance with DVS Guidelines, control of the necessary application temperature using quick-display surface temperature thermometers is permissible.

## WELDING TECHNOLOGY

## 6．2 Processing Information for Welding

Parameters for socket welding with a heated tool
Table 14

| Outer pipe diameter mm | Insertion depth mm | Heating period for SDR 11，SDR 7．4，SDR 6 |  | Processing period （maximum period） <br> S | Cooling period |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | fixed | total |
|  |  | at $20^{\circ}$ | below $+5^{\circ}$ |  | s | min |
| 20 | 14 | 5 | 8 |  | 4 | 6 | 2 |
| 25 | 15 | 7 | 11 | 4 | 10 | 2 |
| 32 | 16.5 | 8 | 12 | 6 | 10 | 4 |
| 40 | 18 | 12 | 18 | 6 | 20 | 4 |
| 50 | 20 | 18 | 27 | 6 | 20 | 4 |
| 63 | 24 | 24 | 36 | 8 | 30 | 6 |
| 75 | 26 | 30 | 45 | 8 | 30 | 6 |
| 90 | 29 | 40 | 60 | 8 | 40 | 6 |
| 110 | 32.5 | 50 | 75 | 10 | 50 | 8 |
| 125 | 35 | 60 | 90 | 10 | 60 | 8 |

Note：heating element temperature 250 to $270^{\circ} \mathrm{C}$

Instructions for socket welding can be found in DVS brochure no．2207，Section 11，＂Socket welding with a heated tool－welding of thermoplastic plastics and pipelines made of polypropylene（PP）＂．POLO－ECOSAN socket welding is performed according to these guidelines．
In this process，pipes and fittings are welded overlapping．The end of the pipes and fittings are heated using a welding device and are subsequently connected．

## WELDING TECHNOLOGY

### 6.2.1 Socket Welding with a Hand-Held Welding Device, from 20 mm

## The following points should be observed:

1. The welding device should be equipped with the appropriate welding tools. Welding bushes and core rods have a Teflon coating. In order to avoid damaging the Teflon coating, never use pliers or similar tools for assembly. Please use a suitable hexagon socket wrench.
2. Switch on the welding device.
3. Using a thermometer or a temperature control pin, check welding temperature before starting to weld.
4. The ends of the pipes must be cut straight. Use appropriate pipe scissors or cutters. Pipe, fittings and welding tools must be clean. If necessary, clean them with a lint-free cloth.
5. Fitting and pipe must be inserted quickly and axially, without twisting, into the corresponding welding tools. The parts to be welded are then heated without pressure according to the table.
6. After the required heating time, fitting and pipe are to be removed quickly from the heating element and connected immediately by pushing together without twisting until insertion depth or markings have been reached. A double roll provides a visual guide to determine the correct welding (see DVS brochure 2207, Section 11). The line markings on the fittings and the pipe ensure the proper alignment of the pipes.
7. Pressure due to subsequent installation works must not be exerted upon the welded connection until after the end of the cooling period.


8. If necessary, clean the welding tools after each use.

## WELDING TECHNOLOGY

## 6．2．2 Socket Welding with a Stationary Welding Machine，from 40 mm

## 6．2．2．1 Area of use

We recommend the use of a stationary welding machine for the welding of larger pipe diameters and for the pre－assembly of installation elements．The general guidelines provided by DVS brochure no．2207，Section 11， ＂Socket welding with a heated tool．Detailed information on welding times．＂apply here．

## 6．2．2．2 Processing Steps

1．Check the machine：Establish welding insertion depth by setting the dimension；make sure the welding temperature is reached．

2．Fix the moulded part with the clamp，taking care not to wind it too tightly，as this can lead to ovality，with a negative impact on the resulting weld．Make sure the moulded part is correctly positioned； use counter－tension to prevent the possibility of slipping．

3．Place the pipe loosely into the jaw chuck．

4．Adjust the dimension using the rotary button，which sets the precise welding insertion depth．

5．Push both tools together until they reach the stop．

6．Push the pipe as far as the fitting，then tighten．Make sure that the welding partners are accurately aligned．Open the welding tool．


7．Insert the welding device．Using the crank，gradually push the fitting and the pipe into the tool until the stop is reached．Pay attention to the welding time．

8．The welding period begins when the pipe and the fitting have been fitted together closely．Allow them to heat up without exerting any further pressure．Once the heating time has elapsed，move the tools apart，remove the welding device，and fit together the fitting and the
 pipe．

9．Observe the required cooling time．


## WELDING TECHNOLOGY

### 6.2.3 Welding Saddle for $40-160 \mathrm{~mm}$

### 6.2.3.1 Area of use

- subsequent extension of existing pipe systems
- alternative use instead of tees
- direct branching of a service line to a supply line
- simple assembly of sensor sleeves


### 6.2.3.2 Processing Steps

1. Before you start the work, prepare material and tools. Ensure that the welding saddle, the drill and the welding tool have the same diameters.
2. Uncover the pipe at the exact location where the welding saddle is supposed to be welded, and mark the welding area. Drain existing pipes and vent the pressure.

3. Prepare the welding device and the saddle welding tools for the polyfusion welding and heat to operating temperature (250-270 ${ }^{\circ} \mathrm{C}$ ).
4. Drill through the marked pipe wall with the POLOPLAST Plastic Drill and clear any cuttings from the drill hole.
5. The parts and areas to be welded must be clean and dry.
6. Push the welding plate into the hole in the wall of the pipe using a
 suitable and aligned saddle tool, until the tool reaches its stop position. At the same time the weld-in saddle must be pushed in, until the saddle surface reaches the camber of the tool.
7. The heating time for the pipe and fittings for the drilled hole dimensions DN 25 and 32 mm is 25 seconds for all dimensions.
8. Once the heating time has elapsed, remove the welding device, push the heated weld-in saddle straight into the heated hole as far
 as it will go without turning it, and hold the pipe in position for at least 20 seconds applying the necessary pressure.
9. After a cooling period of at least 10 minutes, the connection can withstand a full load.


## WELDING TECHNOLOGY

### 6.2.4 Repair Plugs

### 6.2.4.1 Area of use

- the repair of punctured (drilled) pipes


### 6.2.4.2 Processing Steps

1. Drain pipes.
2. Uncover damaged pipe.
3. Drill damaged area of pipe out to a diameter of 8 mm at a right angle to the pipe.
4. Heat up drill hole and repair plug with POLO-ECOSAN hole welding tool for 15 seconds.
5. Insert repair plug immediately.
6. Cut off protruding end of repair plug.
7. The repaired area of pipe has reached full strength after approx. 5 minutes.


## WELDING TECHNOLOGY

### 6.2.5 Use of Electric Welding Sockets

### 6.2.5.1 Area of use

- welding in constrained positions and in areas with restricted space
- repair welding
- alternative processing option for large pipe dimensions


### 6.2.5.2 Preparation

1. General information and controls

Cleanliness - besides the correct operation - is the most important requirement for achieving good welding results! For the sockets to stay thoroughly clean, they need to be left in the original packaging until they are used. Furthermore, the surface of the pipe must be clean and undamaged. Incorrectly collapsed pipe ends must be cut off. We recommend PP-cleaner or cloths with ethyl alcohol for cleaning.

The pipe elements to be welded as well as the electric socket and the welding equipment must show precisely the same temperature level within the permitted temperature range (i.e. $+5^{\circ} \mathrm{C}$ to $40^{\circ} \mathrm{C}$ according to DVS 2207). (UV radiation or improper storage, to name two examples, can cause significant differences in temperature, which will result in faulty welding.)

## 2. Preparatory Work

It is absolutely mandatory to maintain the order of the working steps!

1. Cut pipe ends at a right angle and burr them (control carved ends).
2. Remove any dirt from the pipe ends at the required length and dry them.
3. Mark the insertion depth of the electro-welded sockets at the pipe end.
4. Remove the oxide film with a pipe scraper on the pipe surface
 along the length of the insertion depth. Use the peeler intended for the respective diameter of the pipe.
5. Clean thoroughly using ethyl alcohol. A homogeneous and impermeable welded connection can only be established, if the surface in the welding range is peeled and cleaned comprehensively.

Do not touch peeled pipe ends again and protect them from new contamination - e. g put a clean plastic bag over them. Weld within 30 minutes after the peeling process.

## 3. Assembly of the electric welding socket

1. Carefully clean the inner surface of the socket using lint-free cloth. Mount the socket within 30 minutes after opening the packaging.
2. Slide the electric welding socket onto the clean and dry pipe end until you reach the marked insertion depth.
3. Completely remove the protective foil and slide the peeled and clean second pipe end into the electric welding socket.


## WELDING TECHNOLOGY

Contaminations are to be avoided diligently and all parts must be securely fastened. Pipes must be free of flexural strain or self-weight when they are inserted into the electric welding socket. The socket should still be able move on the pipe ends after the mounting process. The air gap must be evenly distributed around the circumference. A joint that is not free of tension or that has shifted can result in undesired molten mass or in an inadequate connection. The pipe ends and welded sockets must be dry when mounted.
4. Welding process $\mathbf{2 0} \mathbf{- 1 1 0 ~ m m ~ ( a u t o m a t i c ~ s e q u e n c e ) ~}$

1. Position the socket so that the air gap is evenly distributed around the circumference.
2. Insert the plug of the welding equipment into the electric welding socket.
3. Start the welding equipment and follow the automatic sequence.
4. Start the welding process and monitor it closely.
5. Welding process $\mathbf{1 2 5 - 2 5 0 ~ m m ~ ( m a n u a l ~ s e q u e n c e ) ~}$
6. Position the socket so that the air gap is evenly distributed around the circumference.
7. Set the welding equipment to the diameter of the welding socket.
8. Compare the data on the welding equipment's display screen with the details on the label and enter the requested code by scanner or manual (see barcode label on the electric welding socket).
9. Start the welding process and monitor it closely.

The joint must not be moved or put under external pressure during the entire welding process, until it has completely cooled off! Once the welded connection has been successfully established, two pins remains visible as an outward sign (Illustration 1).

## 6. Cooling-off time and pressure test

The welded pipe joint may only be put under pressure or moved, and the fastening may only be loosened once the cooling-off period has elapsed!

(ILLUSTRATION 1)

The minimum required cooling-off time is marked on the electric welding sockets. In case of ambient temperatures above $25^{\circ} \mathrm{C}$ or when there is strong solar radiation, the cooling-off time must be extended accordingly!

In order to achieve an ideal and stable welding result, both pipe ends must be plane-parallel within the electric welding socket! It is imperative to mark the socket insertion depth on the pipe, and to adhere to it!

| Type of strain | Compression strain | Minimum waiting period |
| :--- | :--- | :--- |
| Tension, bending, torsion of unpressurised pipelines |  | 20 minutes |
| Testing or working pressure of pressurised pipelines | up to 0.1 bar | 20 minutes |
|  | 0.1 bar to 1 bar | 60 minutes |
|  | over 1 bar | 120 minutes |
| Repetition of welding process |  | 60 minutes |

## WELDING TECHNOLOGY

### 6.2.6 Butt Welding Process for 160 mm and Above

Please also refer to the operating instructions for your welding equipment, which will provide the precise welding parameters.

## Processing Steps

1. Protect the workplace against the effects of weather and against contamination by dirt.
2. Heat up the welding machine and check for proper function.
3. Cut the pipes at a right angle to the required length.
4. Align the pipes and tighten the clamping elements.
5. Using a milling machine, plane the front of the pipes at a uniform level and evenly.
6. Remove shavings and clean the front side with ethyl alcohol.
7. Maintain pipe offset (at most $0.1 \times$ wall thickness).
8. Combine the pipes and check for a seamless connection (maximum tolerance 0.5 mm ).

9. Set the joining pressure (refer to relevant table in the operating instructions of the welding machine).
10. Check welding temperature $\left(210^{\circ} \mathrm{C}\right)$.
11. Examine cleanliness of heated element before every operation.
12. Initiate welding process by swivelling the heated element and press the pipes onto the heating element using joining pressure.
13. After reaching the bead height, the pressure is reduced. This is the start of the warm-up time, which brings the pipe ends to the required welding temperature.


Once the warm-up time has elapsed, remove the heated element swiftly, and combine the pipes using the necessary pressure.
15. The pipes are now welded and will cool down under pressure.
16. Do not release or remove the welded joint from the clamps until the stipulated cooling-off period has elapsed.



## WELDING TECHNOLOGY

## 6．2．7 Ceiling Welding Machine for 63－125 mm

The advantage of this welding appliance is the simple welding of pipes and moulded parts in areas that are difficult to access， such as in shafts and under ceilings． With the help of the electric ceiling welding machine，POLO－ECOSAN pipes and fittings can be connected with little effort，despite difficult working conditions，as compared to traditional welding methods．

## Processing Steps

1．Mark the welding insertion depth of the fitting on the pipe．

2．Mount the wide seat of the welding equip－ ment on the pipe，maintaining a distance of approx． 1.5 cm to the marking of the welding insertion depth．Mount the narrow seat on the fitting．

3．Set the pipe dimensions on the fastening bracket when you install the pipes，and fasten at both seats．

4．Insert the heated welding plate．

5．Use a cordless screwdriver to fitting with the welding plate onto the pipe．Observe the heating－up time！

6．Use a cordless screwdriver to pull the pipe and the fitting away from the welding plate．

7．Remove welding plate！Use cordless screwdriver to push together pipe and fitting．Only remove clamping jaws once the cooling－off period has elapsed．Observe cooling－off times．

8．Remove welding device from the pipe and the moulded part．

| Dimension <br> $\mathbf{m m}$ | Welding insertion depth <br> $\mathbf{m m}$ | Heating－up time <br> $\mathbf{s}$ | Processing time <br> $\mathbf{s}$ | Cooling－down time <br> min |
| :---: | :---: | :---: | :---: | :---: |
| $\mathbf{6 3}$ | 24.0 | 24 | 8 | 6 |
| $\mathbf{7 5}$ | 26.0 | 30 | 8 | 8 |
| 90 | 29.0 | 40 | 8 | 8 |
| $\mathbf{1 1 0}$ | 32.5 | 50 | 10 | 8 |
| $\mathbf{1 2 5}$ | 35.0 | 60 | 10 | 8 |

## ASSEMBLY GUIDELINES

### 7.1 Fastening Techniques

A pipe fastening system that complies with regulations is subject to the following requirements:

- The fastening system must absorb any forces that may occur.
- The external impact upon pipes and fittings, caused e.g. by sagging, changes in length, mechanical load, must be prevented by applying appropriate fastening techniques.
- The pipework must be held firmly in the intended position.

The fastening mechanism must be selected in accordance with the outside diameter of the pipe due to be fixed into position. Take appropriate measures to ensure that the pipe surface cannot be damaged by any of the pipe fastening elements.

Experience has shown that pipe clamps with rubber inserts represent the ideal fastening mechanism for POLOPLAST installation systems. In the selection of suitable fastening materials, we generally differentiate between fixed bearings and slide or guide bearings.

### 7.1.1 Fix points

Fixed bearings must be calculated in such a way that all occurring forces, in particular tensile forces, can be absorbed without any ensuing damage. For this purpose, the fastening system must be adjusted to the anticipated forces.

Fixtures attached to pipes (e.g. valves and fitting, connections to equipment or machinery) can be regarded as compulsory fixed points, provided that the possibility of pipe movement can be excluded.

The arrangement of the fixed bearings divides the pipeline system into separate line sections, which must absorb the linear expansion. This partitioning is designed to prevent any uncontrolled movements of the pipe and to ensure a reliable pipe routeing.

When using threaded rods or hanger bolts, make sure to maintain a short distance to the ceiling. So-called swinging suspensions are not suitable for fixed bearings.

### 7.1.2 Sliding points

Slide bearings support the pipe and must allow the movement of the pipeline in an axial direction without risk of damage to the pipe. Only the weight forces of the pipe system need to be included in the analysis.

When positioning the slide bearings, make sure that pipeline movement is not obstructed by closely arranged fittings or fixtures.

## ASSEMBLY GUIDELINES

## 7．2 Mounting Distances

Tables for the determination of the distance between clamps，depending on temperature and outside diameter． The values specified are POLOPLAST recommendations，and are valid for horizontal and vertical installations．

POLO－ECOSAN pipes SDR 6，SDR 7．4，SDR 11

| Dimension in mm | Media temperature［ ${ }^{\circ} \mathrm{C}$ ］ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 20 | 30 | 40 | 50 | 60 | 70 |
|  | Mounting distances［cm］ |  |  |  |  |  |  |
| 20 | 80 | 70 | 65 | 65 | 65 | 60 | 60 |
| 25 | 90 | 80 | 75 | 75 | 75 | 70 | 70 |
| 32 | 100 | 90 | 85 | 85 | 85 | 80 | 80 |
| 40 | 110 | 100 | 95 | 95 | 95 | 90 | 90 |
| 50 | 140 | 120 | 115 | 110 | 105 | 100 | 100 |
| 63 | 160 | 140 | 130 | 125 | 120 | 110 | 110 |
| 75 | 180 | 150 | 140 | 135 | 130 | 120 | 120 |
| 90 | 210 | 160 | 150 | 150 | 140 | 130 | 130 |
| 110 | 240 | 180 | 170 | 160 | 150 | 140 | 140 |
| 125 | 260 | 200 | 185 | 170 | 160 | 150 | 150 |

POLO－ECOSAN pipes with pipe supports SDR 6，SDR 7．4，SDR 11

| Dimension in mm | Media temperature $\left[{ }^{\circ} \mathrm{C}\right]$ |  |
| :---: | :---: | :---: |
|  | $\mathbf{1 0}$ | $\mathbf{7 0}$ |
|  | Mounting distances $[\mathrm{cm}]$ |  |
| $\mathbf{2 0}$ | 170 | 150 |
| 25 | 200 | 180 |
| 32 | 220 | 200 |
| $\mathbf{4 0}$ | 230 | 210 |
| $\mathbf{5 0}$ | 230 | 230 |
| $\mathbf{6 3}$ | 230 | 230 |
| $\mathbf{7 5}$ | 230 | 230 |
| 90 | 230 | 230 |
| 110 | 230 | 230 |

## ASSEMBLY GUIDELINES

POLO-ECOSAN ML5 and POLO-ECOSAN ML3 pipes, SDR 7.4, SDR 11

| Dimension in mm | Media temperature [ ${ }^{\circ} \mathrm{C}$ ] |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 20 | 30 | 40 | 50 | 60 | 70 |
|  | Mounting distances [cm] |  |  |  |  |  |  |
| 20 | 110 | 95 | 90 | 85 | 85 | 80 | 70 |
| 25 | 120 | 105 | 105 | 95 | 95 | 90 | 80 |
| 32 | 140 | 120 | 120 | 110 | 110 | 105 | 95 |
| 40 | 160 | 140 | 135 | 125 | 125 | 120 | 110 |
| 50 | 185 | 155 | 155 | 145 | 145 | 135 | 130 |
| 63 | 200 | 175 | 175 | 165 | 165 | 155 | 145 |
| 75 | 215 | 190 | 190 | 175 | 175 | 165 | 155 |
| 90 | 230 | 210 | 210 | 195 | 195 | 180 | 180 |
| 110 | 250 | 220 | 220 | 210 | 200 | 200 | 190 |
| 125 | 250 | 240 | 225 | 215 | 195 | 185 | 170 |
| 160 | 280 | 270 | 245 | 235 | 205 | 195 | 180 |
| 200 | 285 | 275 | 250 | 240 | 210 | 205 | 185 |
| 250 | 290 | 280 | 255 | 245 | 215 | 200 | 190 |

### 7.3 Laying the Pipes

In the case of pipes laid in walls and ceilings, the friction forces that occur prevent the expansion of the pipes, and therefore no compensation is necessary. The resulting tension is absorbed by the pipe materials.

Due to the low expansion forces, the masonry or the plaster are not damaged

## Installing pipes in a shaft

In the case of rising pipes arranged in shafts, care must be taken with each floor junction to ensure that the branch pipe can oscillate sufficiently, in accordance with the variation in length of the rising pipe.

This can be achieved by the optimal positioning of the rising pipe in the shaft (1), by using an adequately sized feeder for the branch pipe (2) or by the addition of a spring
 leg (3).

The correct arrangement of fixed and loose points, taking the bending legs into consideration, allows the straightforward control of expansion in basement pipes and rising pipes.

## Open laying of pipes



The optical design is of particular importance wherever pipes remain exposed after laying. In order to meet these requirements, the length variation of the pipes must be taken into account.

By using pipe supports, bending legs and expansion bends, linear expansion can be managed very easily.


## ASSEMBLY GUIDELINES

## 7．4 Length Variation

Changes in the length of pipes are dependent on the increasing temperature of the pipe material．This tem－ perature change can be caused by different installation and operating temperatures，as well as varying media temperatures．The potential variation in length must be taken into account at the time of installation．

If the operating temperature is higher than the installation temperature，the pipe will elongate．If the media temperature（e．g．cold water）is lower than the installation temperature，the calculation will result in a reduction in length．

The following factors must be considered in the calculation of the variation in length：
－installation temperature
－operating temperatures（media temperatures）
－temperature difference between installation and operating temperatures
－coefficient of linear expansion
－pipe length

The coefficient of linear expansion $\alpha$ for POLO－ECOSAN pipes are：
－POLO－ECOSAN pipe
－POLO－ECOSAN pipe with pipe support
－POLO－ECOSAN ML3 pipe
－POLO－ECOSAN ML5 pipe
$\alpha=0.15 \mathrm{~mm} / \mathrm{mK}$
$\alpha=0.05 \mathrm{~mm} / \mathrm{mK}$
$\alpha=0.05 \mathrm{~mm} / \mathrm{mK}$
$\alpha=0.038 \mathrm{~mm} / \mathrm{mK}$

The formula for the calculation of the variation in length is：

| $\Delta L=\alpha \times I_{0} \mathbf{X} \Delta \mathbf{T}$ |  |  |
| :---: | :---: | :---: |
| $\Delta \mathrm{~L}$ | variation in length | mm |
| $\mathrm{I}_{0}$ | pipe length prior to temperature change | m |
| $\alpha$ | length variation coefficient | $\frac{\mathrm{mm}}{\mathrm{m} \mathrm{x}}$ |
| $\Delta \mathrm{T}$ | maximum occurring temperature <br> difference between installation and operating <br> temperature | K |

Example：
POLO－ECOSAN SDR 6
Length： 14 m
Installation temperature： $20^{\circ} \mathrm{C}$
Operating temperature： $60^{\circ} \mathrm{C}$

$$
\begin{aligned}
& I=0.15 \frac{\mathrm{~mm} \times 14 \mathrm{~m} \times(60-20) \mathrm{K}}{\mathrm{~m} \times \mathrm{K}} \\
& \mathrm{I}=84 \mathrm{~mm}
\end{aligned}
$$

Calculation with ML5 Pipe：
I $=21.28 \mathrm{~mm}$

## ASSEMBLY GUIDELINES

|  | Linear expansion tables |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | POLO-ECOSAN pipe |  |  |  |  |  |  |  |  |
|  | pipe length in meters ( m ) | difference in temperature $\Delta T(K)$ |  |  |  |  |  |  |  |
|  |  | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
|  | 1.0 | 1.5 | 3.0 | 4.5 | 6.0 | 7.5 | 9.0 | 10.5 | 12.0 |
|  | 2.0 | 3.0 | 6.0 | 9.0 | 12.0 | 15.0 | 18.0 | 21.0 | 24.0 |
|  | 3.0 | 4.5 | 9.0 | 13.5 | 18.0 | 22.5 | 27.0 | 31.5 | 36.0 |
|  | 4.0 | 6.0 | 12.0 | 18.0 | 24.0 | 30.0 | 36.0 | 42.0 | 48.0 |
|  | 5.0 | 7.5 | 15.0 | 22.5 | 30.0 | 37.5 | 45.0 | 52.5 | 60.0 |
|  | 6.0 | 9.0 | 18.0 | 27.0 | 36.0 | 45.0 | 54.0 | 63.0 | 72.0 |
|  | 7.0 | 10.5 | 21.0 | 31.5 | 42.0 | 52.5 | 63.0 | 73.5 | 84.0 |
|  | 8.0 | 12.0 | 24.0 | 36.0 | 48.0 | 60.0 | 72.0 | 84.0 | 96.0 |
|  | 9.0 | 13.5 | 27.0 | 40.5 | 54.0 | 67.5 | 81.0 | 94.5 | 108.0 |
|  | 10.0 | 15.0 | 30.0 | 45.0 | 60.0 | 75.0 | 90.0 | 105.0 | 120.0 |
|  | 15.0 | 22.5 | 45.0 | 67.5 | 90.0 | 112.5 | 135.0 | 157.5 | 180.0 |
|  | 20.0 | 30.0 | 60.0 | 90.0 | 120.0 | 150.0 | 180.0 | 210.0 | 240.0 |
|  | 25.0 | 37.5 | 75.0 | 112.5 | 150.0 | 187.5 | 225.0 | 262.5 | 300.0 |
|  | 30.0 | 45.0 | 90.0 | 135.0 | 180.0 | 225.0 | 270.0 | 315.0 | 360.0 |
|  | 35.0 | 52.5 | 105.0 | 157.5 | 210.0 | 262.5 | 315.0 | 367.5 | 420.0 |
|  | 40.0 | 60.0 | 120.0 | 180.0 | 240.0 | 300.0 | 360.0 | 420.0 | 480.0 |
|  | 45.0 | 67.5 | 135.0 | 202.5 | 270.0 | 337.5 | 405.0 | 472.5 | 540.0 |
|  | 50.0 | 75.0 | 150.0 | 225.0 | 300.0 | 375.0 | 450.0 | 525.0 | 600.0 |
|  | linear expansion $\Delta L$ in mm |  |  |  |  |  |  |  |  |
|  | POLO-ECOSAN pipe with pipe support, POLO-ECOSAN ML3 |  |  |  |  |  |  |  |  |
|  | pipe length in meters ( m ) | difference in temperature $\Delta T(K)$ |  |  |  |  |  |  |  |
|  |  | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
|  | 1.0 | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.5 | 4.0 |
|  | 2.0 | 1.0 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 7.0 | 8.0 |
|  | 3.0 | 1.5 | 3.0 | 4.5 | 6.0 | 7.5 | 9.0 | 10.5 | 12.0 |
|  | 4.0 | 2.0 | 4.0 | 6.0 | 8.0 | 10.0 | 12.0 | 14.0 | 16.0 |
|  | 5.0 | 2.5 | 5.0 | 7.5 | 10.0 | 12.5 | 15.0 | 17.5 | 20.0 |
|  | 6.0 | 3.0 | 6.0 | 9.0 | 12.0 | 15.0 | 18.0 | 21.0 | 24.0 |
|  | 7.0 | 3.5 | 7.0 | 10.5 | 14.0 | 17.5 | 21.0 | 24.5 | 28.0 |
|  | 8.0 | 4.0 | 8.0 | 12.0 | 16.0 | 20.0 | 24.0 | 28.0 | 32.0 |
|  | 9.0 | 4.5 | 9.0 | 13.5 | 18.0 | 22.5 | 27.0 | 31.5 | 36.0 |
|  | 10.0 | 5.0 | 10.0 | 15.0 | 20.0 | 25.0 | 30.0 | 35.0 | 40.0 |
|  | 15.0 | 7.5 | 15.0 | 22.5 | 30.0 | 37.5 | 45.0 | 52.5 | 60.0 |
|  | 20.0 | 10.0 | 20.0 | 30.0 | 40.0 | 50.0 | 60.0 | 70.0 | 80.0 |
|  | 25.0 | 12.5 | 25.0 | 37.5 | 50.0 | 62.5 | 75.0 | 87.5 | 100.0 |
|  | 30.0 | 15.0 | 30.0 | 45.0 | 60.0 | 75.0 | 90.0 | 105.0 | 120.0 |
|  | 35.0 | 17.5 | 35.0 | 52.5 | 70.0 | 87.5 | 105.0 | 122.5 | 140.0 |
|  | 40.0 | 20.0 | 40.0 | 60.0 | 80.0 | 100.0 | 120.0 | 140.0 | 160.0 |
|  | 45.0 | 22.5 | 45.0 | 67.5 | 90.0 | 112.5 | 135.0 | 157.5 | 180.0 |
|  | 50.0 | 25.0 | 50.0 | 75.0 | 100.0 | 125.0 | 150.0 | 175.0 | 200.0 |
|  |  | linear expansion $\Delta L$ in mm |  |  |  |  |  |  |  |

## ASSEMBLY GUIDELINES

| POLO－ECOSAN ML5．POLO－UV ML5 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| pipe length | difference in temperature $\Delta \mathrm{T}(\mathrm{K})$ |  |  |  |  |  |  |  |
| in meters（m） | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
| 1.0 | 0.4 | 0.8 | 1.1 | 1.5 | 1.9 | 2.3 | 2.7 | 3.0 |
| 2.0 | 0.8 | 1.5 | 2.3 | 3.0 | 3.8 | 4.6 | 5.3 | 6.1 |
| 3.0 | 1.1 | 2.3 | 3.4 | 4.6 | 5.7 | 6.8 | 8.0 | 9.1 |
| 4.0 | 1.5 | 3.0 | 4.6 | 6.1 | 7.6 | 9.1 | 10.6 | 12.2 |
| 5.0 | 1.9 | 3.8 | 5.7 | 7.6 | 9.5 | 11.4 | 13.3 | 15.2 |
| 6.0 | 2.3 | 4.6 | 6.8 | 9.1 | 11.4 | 13.7 | 16.0 | 18.2 |
| 7.0 | 2.7 | 5.3 | 8.0 | 10.6 | 13.3 | 16.0 | 18.6 | 21.3 |
| 8.0 | 3.0 | 6.1 | 9.1 | 12.2 | 15.2 | 18.2 | 21.3 | 24.3 |
| 9.0 | 3.4 | 6.8 | 10.3 | 13.7 | 17.1 | 20.5 | 23.9 | 27.4 |
| 10.0 | 3.8 | 7.6 | 11.4 | 15.2 | 19.0 | 22.8 | 26.6 | 30.4 |
| 15.0 | 5.7 | 11.4 | 17.1 | 22.8 | 28.5 | 34.2 | 39.9 | 45.6 |
| 20.0 | 7.6 | 15.2 | 22.8 | 30.4 | 38.0 | 45.6 | 53.2 | 60.8 |
| 25.0 | 9.5 | 19.0 | 28.5 | 38.0 | 47.5 | 57.0 | 66.5 | 76.0 |
| 30.0 | 11.4 | 22.8 | 34.2 | 45.6 | 57.0 | 68.4 | 79.8 | 91.2 |
| 35.0 | 13.3 | 26.6 | 39.9 | 53.2 | 66.5 | 79.8 | 93.1 | 106.4 |
| 40.0 | 15.2 | 30.4 | 45.6 | 60.8 | 76.0 | 91.2 | 106.4 | 121.6 |
| 45.0 | 17.1 | 34.2 | 51.3 | 68.4 | 85.5 | 102.6 | 119.7 | 136.8 |
| 50.0 | 19.0 | 38.0 | 57.0 | 76.0 | 95.0 | 114.0 | 133.0 | 152.0 |
| linear expansion $\Delta \mathrm{L}$ in mm |  |  |  |  |  |  |  |  |

## 7．5 Thermal Expansion Force

The following formula can be used to calculate the thermal expansion force：
$F_{t}=\frac{E \times A \times \alpha \times \Delta T}{1000}$
$\mathrm{F}_{\mathrm{t}}=$ thermal expansion force［ N ］
$E=$ modulus of elasticity（modulus of rigidity）$\left[\mathrm{MPa}=\mathrm{N} / \mathrm{mm}^{2}\right]$
A $=$ cross－sectional area of the pipe in［ $\mathrm{mm}^{2}$ ］
$\alpha=$ specific thermal expansion coefficient $[\mathrm{mm} /(\mathrm{mK})]$
$\Delta T=$ temperature difference resulting from media temperature minus laying temperature $[K]$

| Material | Pipe dimension | Modulus of elasticity | Coefficient of linear <br> expansion | Thermal Expansion Force |
| :---: | :---: | :---: | :---: | :---: |
| Steel | $26.9 \times 2.65$ | 220,000 | 0.012 | 533 |
| High－grade steel | $22.0 \times 1.2$ | 200,000 | 0.015 | 235 |
| Copper | $22.0 \times 1.0$ | 130,000 | 0.016 | 137 |
| Prostab | $25.0 \times 3.5$ | 3,500 | 0.035 | 29 |
| PVC | $25.0 \times 3.2$ | 1,100 | 0.08 | 19 |
| PP－R／PP RCT | $25.0 \times 4.2$ | 900 | 0.150 | 12 |
| PE－X | $25.0 \times 3.5$ | 540 | 0.175 | 22 |
| PE－RT | $25.0 \times 3.5$ | 250 | 0.180 | 10 |
| PE－X／Alu | $26.0 \times 3.0$ | 3,500 | 0.030 | 22 |

## ASSEMBLY GUIDELINES

This comparison shows that the thermal expansion forces occurring in plastic pipes are extremely low, compared to pipes made of metallic materials

If the thermal expansion force is countered by a corresponding retention force, the expansion can be neutralised effectively.


### 7.6 Expansion Compensation

Variations in length caused by temperature differences must be taken into account during the planning stage to prevent subsequent damage to pipelines, fastening elements and the building structure. In order to keep the occurring stress impacts within acceptable ranges, the variation in length must be compensated appropriately. There are two options available to achieve this compensation:

- Expansion compensation using bending legs and a U-pipe bends ("natural" expansion compensation)
- Expansion compensation using compensators ("artificial" expansion compensation)

In most cases, directional changes in the pipe routeing can be utilised to absorb the variation in length. Should the directional changes not be sufficient, a U-pipe bend must be used.

It is important to bear in mind that the outlets distributed throughout the line system can also influence the variation in length, or may be negatively affected themselves by the variation in length.

Please refer to the manufacturers of the compensators for more information on the expansion compensation provided by compensators.

### 7.6.1 Bending Legs

In order to determine the specific direction in which the expansion compensation is steered, the directional change is installed between two fixed points. Generally, the pipes are arranged in right angles at the points where the direction changes. A variation in the length of one leg produces bending in the other leg. Provided that all legs are of a sufficient length to prevent the resulting flexural strain from becoming too great, the system can flexibly absorb the variation in length.

| $I_{B}=K \times \sqrt{\mathbf{d x \Delta L}}$ |  |  |
| :---: | :---: | :---: |
| $I_{B}$ | length of the bending leg | mm |
| $K$ | material-dependent constant (15.0 for PP) |  |
| $d$ | outside pipe diameter | mm |
| $\Delta L$ | variation in length | mm |

## Sample calculation:

Pipe outside diameter 75 mm
Variation in length 84 mm

```
I
I}=1191\textrm{mm
```


## ASSEMBLY GUIDELINES

## 7．6．2 Expansion Loop

If it is not possible to compensate for the variation in length by introducing directional changes into the pipe routeing，an expansion loop must be used instead．
For the implementation of the expansion bend，the length $l_{B}$ of the bending leg and the width $b_{\text {min }}$ of the expansion bend must be considered．It is advisable to position the expansion bend in such a way that the lengths $I_{1}$ and $I_{2}$ are equal．

| $\mathbf{b}_{\min }=\mathbf{2} \times \Delta \mathbf{L}+\mathbf{S A}$ |  |  |
| :---: | :---: | :---: |
| $\mathrm{b}_{\min }$ | minimum width of the expansion | mm |
| $\Delta \mathrm{L}$ | variation in length | mm |
| SA | safety clearance $=150$ | mm |

Sample calculation：
Variation in length $\Delta L=84 \mathrm{~mm}$

$$
\begin{aligned}
& \mathrm{b}_{\min }=2 \times 84 \mathrm{~mm}+150 \mathrm{~mm} \\
& \mathrm{~b}_{\min }=318 \mathrm{~mm}
\end{aligned}
$$


length variation and is thus＂pre－tensioned＂，the length of the bending leg $l_{\mathrm{BV}}$ can be reduced．

| $I_{B V}=I_{\mathbf{B}} \mathbf{X} \sqrt{1-\frac{\Delta L_{V}}{\Delta L}}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\Delta L_{V}$ | variation in length with pre－tensioning | mm |  |  |
| $\Delta L$ | variation in length | mm |  |  |
| $\mathrm{I}_{B V}$ | length of bending leg with pre－tensioning | mm |  |  |
| $\mathrm{I}_{\mathrm{B}}$ | length of bending leg | mm |  |  |

Sample calculation：
Variation in length $\Delta L=84 \mathrm{~mm}$
Pre－tensioning $\Delta L_{V}=42 \mathrm{~mm}$

$$
\begin{aligned}
& I_{\mathrm{BV}}=1191 \mathrm{~mm} \sqrt{\times 1-\frac{42}{84} \mathrm{~mm}} \\
& \mathrm{I}_{\mathrm{BV}}=842 \mathrm{~mm}
\end{aligned}
$$



## ASSEMBLY GUIDELINES

### 7.7 Insulation

The EnEV (German Energy Saving Regulation) standard regulates the thermal insulation of pipelines and fittings within the Federal Republic of Germany. The tasks of a pipe insulation are:

- Protect the pipes against condensation
- Protect the cold water pipes against exposure to heat
- Minimize heat losses
- Reduce the transfer of heat to structural components
- Reduce sound transmission
- Protect against UV radiation
- Absorb variations in length caused by temperature
- Protect against mechanical stresses
- Protect against corrosion


### 7.7.1 Hot Water Insulation

## Requirements according to EnEV

Table 15: Thermal insulation of heat distribution and hot water pipelines as well as fittings.

| Line | Type of pipeline / valves and fittings | Minimum thickness of the insulation layer, based on a thermal conductivity of $0.035 \mathrm{~W} /(\mathrm{m} \mathrm{k})$ |
| :---: | :---: | :---: |
| 1 | Inner diameter up to 22 mm | 20 mm |
| 2 | Inner diameter above 22 mm up to 35 mm | 30 mm |
| 3 | Inner diameter above 35 mm up to 100 mm | equal to inner diameter |
| 4 | Inner diameter above 100 mm | 100 mm |
| 5 | Pipes, valves and fittings acc. to lines 1 to 4 in wall and ceiling breaks, at the intersection of lines, at line connection points, at central mains system switches | 1/2 of the requirements listed in lines 1 to 4 |
| 6 | Central heating pipes acc. to lines 1 to 4 , that have been installed in buildings between heated rooms of various users since January 31, 2002 | $1 / 2$ of the requirements listed in lines 1 to 4 |
| 7 | Pipes acc. to line 6 installed in floor constructions | 6 mm |
| 8 | Cold distribution and cold water pipes as well fittings for ventilation and cooling systems | 6 mm |

When using materials with thermal conductivity values other than $0.035 \mathrm{~W} /(\mathrm{m} \mathrm{K})$, the minimum thickness values of the insulation layers must be converted accordingly. The calculation methods and values contained within accepted engineering standards must be employed for the conversion and the thermal conductivity of the insulation material.

In the case of heat distribution and hot water pipes, as well as cold distribution and cold water pipes, the minimum thickness values of the insulation layers listed in Table 5 may be reduced to the extent of the equivalent limitation of heat absorption or loss, and the insulating effect of the pipe walls must be taken into account.

## ASSEMBLY GUIDELINES

### 7.7.2 Cold Water Insulation

Guide values for the minimum thickness of insulating layers used to insulate cold drinking water systems against heat and condensation.

Insulation layer thickness acc. to DIN 1988-200, Table 16
Table 16

| Installation situation | Insulation layer thickness at $\boldsymbol{\lambda}=\mathbf{0 . 0 4 0} \mathbf{W} / \mathbf{m K}^{\boldsymbol{*}}$ |
| :--- | :---: |
| Exposed pipes in unheated rooms (e.g. basement) | 9 mm |
| Exposed pipes in heated rooms | 13 mm |
| Pipes installed in a duct, without pipes carrying high-temperature media | 13 mm |
| Pipes installed in a duct, alongside pipes carrying high-temperature media | 13 mm |
| Pipes installed in wall slots, rising pipes | 4 mm |
| Pipes installed in wall recesses, alongside pipes carrying high-temperature media | 13 mm |
| Pipes installed on concrete floor (also alongside non-circulating hot water lines) | 4 mm |

*) If materials with different thermal conductivity coefficients are used, the insulation layer thickness must be converted accordingly in relation to a pipe diameter of $d=20 \mathrm{~mm}$.

The temperature increase of drinking water is primarily influenced, by the duration of stagnation, the position and arrangement of the pipes, and by the insulation used. Care must be taken during installation of pipelines to maintain a sufficient distance to all heat sources such as warm pipes, flues, and heating pipes.

In the case of standing water, even insulation measures cannot provide long-term protection against warming.

### 7.7.3 Dew Point

Condensation occurs when the temperature of a surface falls below the saturation temperature of the surrounding air.
The saturation temperature of the air is determined from the current temperature and the relative humidity. The temperature of the surface is determined by the heat transfer from the material to the pipe surface, from the air to the pipe surface, and the heat transfer through the pipe wall.

## Data required in order to determine the dew point:

- Relative air humidity
- Room temperature
- Water temperature
- Temperature difference $\Delta \vartheta$ in K (room temperature - water temperature)


## Sample calculation:

At an room temperature of $27^{\circ} \mathrm{C}, 60 \%$ relative humidity and $12{ }^{\circ} \mathrm{C}$ water temperature the pipe begins to sweat.

- For SDR 6 pipes the maximum temperature difference is 15 K .
- For SDR 11 pipes the maximum temperature difference is 11 K .


## ASSEMBLY GUIDELINES

Diagram for the determination of the dew point for POLO-ECOSAN SDR 6

Diagram for the determination of the dew point for POLO-ECOSAN SDR 11


## ASSEMBLY GUIDELINES

## 7．8 Noise Protection

In order to prevent the transmission of structure－borne noise from the pipe system to the building，sound insulation preventing structure－borne sound must be applied to the pipes．This can be achieved through tape bindings，insulating hoses or through sheathed half－shells．This type of insulation dampens the transmission of flow noise as well as noises from machine parts（pumps）to the structural components surrounding the pipes． Standard DIN 4109 with Supplementary Table A1 regulates the minimum requirements of sound insulation in buildings，given varying requirements and taking into account the source of noise．The following sound pressure levels in $\mathrm{dB}(\mathrm{A})$ are admissible．

Admissible sound pressure levels in rooms requiring sound protection against noise from building services and commercial enterprises

| Source of noise | Characteristic sound pressure level $\mathrm{dB}(\mathrm{A})$ in |  |
| :---: | :---: | :---: |
|  | Living rooms and bedrooms | Teaching and working spaces |
| Plumbing applications （both water supply－and wastewater systems） | $\leq 30{ }^{17)}$ | $\leq 35^{17}{ }^{2}$ |
| Other building services systems | $\leq 30^{3)}$ | $\leq 35^{3)}$ |
| Businesses during the day 6 a．m．to 10 p．m． | $\leq 35$ | $\leq 35^{3)}$ |
| Businesses during the night 10 p．m．to 6 a．m． | $\leq 25$ | $\leq 35{ }^{3}$ |

${ }^{1)}$ Single，short－term spikes that occur when operating valves and devices in accordance with Table 6 DIN 4109 （opening，closing，adapting，inter－ rupting，etc．）can be disregarded at this time．
${ }^{2)}$ Conditions stipulated in the contract for work to meet the admissible installation sound pressure level：
－The construction documents must take into account the requirements of noise protection，which means that－amongst other requirements to be observed－the necessary sound insulation certificates must be provided for the components used．
－Furthermore，construction management must be named and involved before an installation is closed in or covered．Further details are regulated by the ZVSHK Bulletin（Central Association for Plumbing，Heating，Air Conditioning）．
${ }^{3)}$ In the case of ventilation systems the values are permitted to be $5 \mathrm{~dB}(\mathrm{~A})$ higher，provided that the noise is constant noise，without distinct audible sounds．

## ASSEMBLY GUIDELINES

### 7.9 Fire Protection

The POLO-ECOSAN installation system is classified as follows:

| Standard | Classification |
| :---: | :---: |
| EN 13501 | E |
| DIN 4102 | B2 |

## EN 13501 and DIN 4102

These standards define the classification of those materials, which are used as products or as product components in building construction. The fire behaviour of the products used is tested and classified by testing the behaviour in the case of fire, e.g. the development and spread of fire and smoke.

## The behaviour of PP-R in the case of fire

Pipes and fittings made of PP-R, PP-RCT and with fibres, do not exhibit an increased conflagration gas toxicity. In construction objects with a greater need for fire protection measures, pipe ducts through walls and ceilings must be protected against fire in such a way that, as a general principle, all pipe ducts have the same classification as the structural components through which the ducts lead.

For example: In the case of a wall, which features a fire resistance period of 90 minutes (F90), the pipe ducting must also have a fire resistance period of 90 minutes (R90).

All fire protection systems that have been issued with a corresponding accreditation can be used with POLO-ECOSAN pipes.

One possible solution is the fire protection measure using fire protection collars or special mineral insulation with a melting temperature of $>1000^{\circ} \mathrm{C}$.


## Fire load

Table 17
The resulting combustion heat $\mathrm{V}(\mathrm{kWh} / \mathrm{m})$ of POLO-ECOSAN pipes is dependent on the pipe dimension. The basis for the calculation of the combustion heat V for POLO-ECOSAN pipes made of PP-R is given by the lower calorific value $\mathrm{Hu}=12.2 \mathrm{kWh} / \mathrm{kg}$ (acc. to DIN 18230 Section 1), as well as the material mass $\mathrm{m}(\mathrm{kg} / \mathrm{m})$.

Combustion values $\mathrm{V}(\mathrm{kWh} / \mathrm{m})$ of POLO-ECOSAN pipes, Table 17

| Outer <br> diameter | PP R |  |  |
| :---: | :---: | :---: | :---: |
|  | SDR 11 | SDR 6 | SDR 7.4 |
| $\mathbf{2 0}$ | 1.31 | 2.1 | 1.80 |
| $\mathbf{2 5}$ | 2 | 3.25 | 2.79 |
| $\mathbf{3 2}$ | 3.25 | 5.3 | 4.44 |
| $\mathbf{4 0}$ | 5.03 | 8.19 | 6.95 |
| $\mathbf{5 0}$ | 7.78 | 12.81 | 10.84 |
| $\mathbf{6 3}$ | 12.32 | 20.13 | 17.05 |
| $\mathbf{7 5}$ | 17.32 | 28.55 | 24.25 |
| $\mathbf{9 0}$ | 24.77 | 41 | 34.76 |
| $\mathbf{1 1 0}$ | 36.72 | 61.49 | 51.88 |
| $\mathbf{1 2 5}$ | 47.54 | 77.84 |  |

## INITIAL OPERATION

### 8.1 Pressure tests

Upon completion of the installation work, drinking water installations inside buildings must be subjected to hydraulic pressure testing. This must be carried out while the pipe system is fully accessible. In accordance with DIN EN 806, the test can be carried out using water or, if national regulations permit, with oil-free clean air at low pressure or inert gases.
The choice of method to be applied must take into account the factors relating to hygiene and corrosion, and must be determined in relation to the design of the system and the time schedule of the construction project.

In order to pressure test using water, the completed pipelines must be gradually filled with drinking water that does not contain particles $\geq 150 \mu \mathrm{~m}$, and must then be vented. The drinking water system must be put into operation immediately after the pressure test with water and the subsequent flushing of the system. If this is not possible, the flushing process must be repeated regularly, with no more than 7 days between repetitions. If the system is due to be put into operation at a later stage, in the interest of hygiene, the pressure test should be conducted with air or inert gas as a testing medium.

Due to the characteristic properties of the materials used, plastic pipes expand for a limited period of time when they are subjected to pressure. This has an impact on the test result. A change in the temperature in a pipe system can lead to a change in pressure in the case of pipes made of plastic.
Consequently, pressure testing should follow the protocols provided below (page 86 and following).

Once the pressure tests have been completed, the responsible technician must produce a formal record, which includes an assessment of the test. The impermeability of the system must be evident, and must be confirmed in writing.

## Pressure Testing with Water

DIN EN 806-4 stipulates that there are three possible pressure tests, depending on the different material properties. Due to issues concerning the practical feasibility on site, and following practical experiments, a modified method was selected, which is suitable for all materials and all material combinations.
The duration of the test was extended beyond the period stipulated in the standard, to ensure that even the smallest possible leaks can be detected during the leak test.

## Pressure Testing with Air

As gases are compressible, when carrying out pressure testing using air, the accident prevention regulations "Working on Gas Installations" and the guidelines "Technical Rules for Gas Installations DVGW-TRGI" must be observed for physical and safety reasons. Therefore, acting in agreement with the responsible professional association and in observance of this body of rules, the testing pressures were fixed at a maximum of 0.3 MPa (3bar), corresponding to the stress and leak tests for gas lines. This fully complies with the national regulations.

The volume in the pipe system has a significant impact on the pressure results shown. Changes in temperature can also influence the test results. A high pipe system volume can have a negative impact on the determination of minor leaks using drops in pressure. Consequently, it can be helpful to divide the test into small sections, in order to achieve the best possible testing safety and accuracy.

```
Pressure Testing Protocol Testing Media Water
Construction project:
``` \(\qquad\)
```

Construction stage:

``` \(\qquad\)
```

Client represented by:

``` \(\qquad\)
```

Contractor represented by:

``` \(\qquad\)
```

Admissible operating pressure $=10$ bar

``` \(\qquad\)
``` bar (if higher)
Water temperature .......... \({ }^{\circ} \mathrm{C} \quad\) Room temperature .......... \({ }^{\circ} \mathrm{C}\)
System inspection as
```

```complete system
```

```in
``` \(\qquad\)
``` sections
```


## Preliminary arrangements:

```
\(\square\) The pipe system is made of PP, PE, PE-X, PB, and with combined installations made of metal and multi-layer composite pipelines.
```

```All pipes have been sealed with metal plugs, caps, blanking plates or blank flanges.
```

```Equipment, pressure tanks or drinking water heaters have been disconnected from the system.
```

```A visual inspection ensuring the professional execution of all pipe connections has been carried out.
```

```Filling water has been filtered. Filter size < \(150 \mu \mathrm{~m}\)
```

```The drinking water system has bee filled, flushed and de-aerated.
```


## Leak test

```
1. Establish testing pressure
``` \(\qquad\)
``` bar \(^{11}(\min 1,1 \times\) admissible operating pressure = 11 bar\()\)
2. In the case of large temperature differences ( \(>10 \mathrm{~K}\) ) between ambient temperature and the filling water, a 30-minute waiting period must be observed after testing pressure has been reached in order to achieve temperature equalization.
3. Testing period: 30 minutes
4. Use visual inspection and pressure gauge to check for obvious leaks.
5. Reduce pressure to 0.5 of testing pressure (e.g. from 11 bar to 5.5 bar)
6. Additional testing period: 120 minutes
7. Assessment:
No drop in pressure ( \(=0\) ) occurred during this period
\(\square\) Visual inspection of pipe system has been carried out
```

```No leaks were determined during the testing period
```

```The pipe system is leak-proof
```

$\qquad$
Place Date

Client
Contractor

1) The pressure gauges used must allow a precise reading of a 0.1 bar change in pressure.

## INITIAL OPERATION

## Pressure Testing Protocol Testing Media Compressed Air or Inert Gas

Construction project： $\qquad$
Construction stage： $\qquad$
Client represented by： $\qquad$
Contractor represented by： $\qquad$
Pipe system materials： $\qquad$
System operating pressure $\qquad$ bar Room air temperature $\qquad$ ${ }^{\circ} \mathrm{C}$

Temperature of testing medium $\qquad$ ${ }^{\circ} \mathrm{C}$

Testing medium $\square$ oil－free compressed air $\square$ nitrogen $\square$ carbon dioxide
System inspection ascomplete systemin $\qquad$ sections

Preliminary arrangements：All pipes have been sealed with metal plugs，caps，blanking plates or blank flanges．Equipment，pressure tanks or drinking water heaters have been disconnected from the system．A visual inspection ensuring the professional execution of all pipe connections has been carried out．

## 1．Leak test ${ }^{1)}$

Testing pressure 150 mbar
Up to 100 litres pipe system capacity require a testing period of at least 120 minutes．For every further 100 litres，the testing period must be extended by 20 minutes．

Pipe system capacity：．．．．．．．．．．litres Testing period：．．．．．．．．．．minutes
The testing period starts，once the testing pressure has been reached，taking into account a waiting period for the equalization of the media temperature and the ambient temperature．Visual inspection of pipe system has been carried outInspection by pressure gauge，U－pipe or respectively standpipe water column has been carried out ${ }^{1)}$No drop in pressure was determined during the testing periodNo leaks were determined during the testing period

## 2．Strength test with elevated pressure ${ }^{2)}$

Wait for temperature equalization and steady state in the case of plastic pipes；the testing period starts once these have been reached．
Testing pressure $\leq 63 \mathrm{~mm}$ maximum 3 bar Testing pressure $>63 \mathrm{~mm}$ maximum 1 bar Testing period： 10 minutesNo drop in pressure was determined during the testing periodNo leaks were determined during the testing periodThe pipe system is leak－proof

[^2]
## INITIAL OPERATION

## 8．2 Flushing the System

On principle，drinking water installations must be thoroughly flushed immediately upon completion， irrespective of the materials used．Flushing the system ensures that the following requirements are observed：
－Protection of drinking water quality
－Prevention of corrosion damage
－Prevention of functional damage to vales，fittings and equipment
－Cleaning of the inner surface of the pipes

According to EN 806－4＂Specifications for installations inside buildings conveying water for human consumption＂，it is necessary to flush the system for drinking water installations as soon as possible upon completion and immediately before putting them into operation．The following regulations must be observed．
－Perform the flushing on warm and cold water systems separately．
－The water must be filtered．The water must not contain any particles＞ $150 \mu \mathrm{~m}$ ，as these can cause
－damage to the system．
－If the system is not put into operation immediately after the system is flushed，the flushing process
－must be repeated regularly，with no more than 7 days between repetitions．

Two flushing methods have proven successful in practice：
1．Flushing with water
2．Flushing with a water／air mixture

The following factors must be considered when applying method＂1．Flushing with water＂：
－Jet regulators，sieves，flow regulators，shower heads or hand－held showers must be dismantled in order to protect them from damage and soiling，and to ensure the maximum possible flow through the pipes．
－All valves and shutoff devices must be fully opened．
－If the system rinse is carried out in sections，it must be started on the lowest floor and continued upwards， moving from floor to floor．
－During the rinsing process the minimum flow rate must be $2 \mathrm{~m} / \mathrm{s}$ ．
－The water content of the system must be completely exchanged at least 20 times．
－When opening the draw－off points，the first draw－off point to be opened must be the one furthest away from the rising pipe．
－Draw－off points are closed in the reverse order：moving from the rising pipe to the end．
－Each draw－off point must be fully opened．

## 8．3 Initial Operation

－Do not fill the system with water until standard operation is imminent．
－Delays cause a hygienic risk．Flushing schedules or forced flushing should be carried out to ensure that the water is exchanged regularly．
－The operator should receive the basic planning documents，the records of leak and stress tests，as well as all flushing and training documents at the same time as the operating instructions．
－The operator must be informed that the regular exchange of the water must be ensured．
－The operator must be advised of the dangers presented by a microbiological contamination of then system caused by hot water temperatures that are too low，and cold water temperatures that are too high．
－The operator should be offered a maintenance contract．

## INITIAL OPERATION

## Initial Operation Protocol: Flushing with water

Construction project: $\qquad$
Construction stage: $\qquad$
Client represented by: $\qquad$
Contractor represented by: $\qquad$
Pipe system materials: $\qquad$
Guide values for the minimum number of draw-off points to be opened, with reference to the largest nominal width of the distribution pipe

| Largest nominal width of the distribution pipe <br> DN in the current flushing section | 25 | 32 | 40 | 50 | 65 | 80 | 100 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum number of draw-off points to be <br> opened DN 15 | 2 | 4 | 6 | 8 | 12 | 18 | 28 |

## Preliminary arrangements:

$\square$ Water for flushing has been filtered. Filter size $<150 \mu \mathrm{~m}$
$\square$ Jet regulators, sieves, flow regulators, hand-held showers, shower heads have been dismantledMaintenance fittings (main shutoff device on each floor and other shutoff devices) have been fully openedSensitive valves, fittings and equipment have been removed and replaced with adaptors
Sequence of the flushing process:

1. The flushing process is carried out in sections, starting at the main shutoff valve and moving towards the furthest draw-off point.
2. On each floor, those draw-off points located furthest away from the rising pipe are fully opened first.
3. All draw-off points are fully opened.
4. After a minimum rinsing period of 5 min (measured from the valve opened last) all draw-off points are closed in reverse order.

Start of the flushing process: $\qquad$
$\square$ Built-in filters and strainers have been cleaned
The flushing of the drinking water system has been properly carried out.

Place Date

## QUALITY MANAGEMENT

### 9.1 Quality Assurance

All incoming goods that are intended for use as raw and auxiliary materials for further processing, are checked for their suitability by POLOPLAST Quality Assurance.

The manufacture of quality-controlled pipeline systems requires all necessary procedural steps:

- Monitoring
- Control
- Inspection

Furthermore, all results and procedures are documented.

The minimum requirements for independent company quality control are derived from the corresponding regulations for the quality control of sanitary pipeline systems, in that compliance must also include inspection by a neutral testing institution within the framework of external control.

External control, in addition to external testing of products, includes

- testing of the manufacturer's own required control measures
- examination of the technical equipment requirements
- hygienic and toxicological testing

External control of approvals for foreign usage is conducted in a similar manner.

The suitability of the POLOPLAST pipe systems for drinking water has been established by the Technology Water Centre (TWZ) according to the "Guideline for Hygienic Assessment of Organic Materials in Contact with Drinking Water" (KTW Guideline) provided by the German Federal Environmental Agency, and is subject to permanent external control.

## Summary of key points:

- The entire production process is defined, monitored, documented
- Quality management according to DIN EN ISO 9001
- Complies with all applicable standards, laws and regulations
- Monitoring by external institutes
- Certified system


## QUALITY MANAGEMENT

## Quality Assurance

The entire production process for POLOPLAST pipe systems and fittings is monitored and controlled by POLOPLAST Quality Assurance．All results and procedures are documented．The monitoring is carried out by external institutes and by self－monitoring．


| External monitoring |
| :---: |
| $\downarrow$ |
| by authorised testing institutes of the DVGW： <br> －Süddeutsches Kunststoffzentrum（Southern German Plastics Centre）（SKZ） <br> －Technologiezentrum Wasser（Technology Centre Water）in Karlsruhe |
| $\downarrow$ |
| Tasks |
| $\downarrow$ |
| －Testing of the manufacturer＇s self－monitoring <br> －Product testing <br> －Examination of the technical equipment requirements <br> －Hygienic and toxicological testing acc．to KTW guidelines |

Our Quality Management system is certified in accordance with DIN EN ISO 9001


In the area of Quality Management，POLOPLAST is certified in accordance with DIN EN ISO 9001.

## QUALITY MANAGEMENT

### 9.1.1 Approvals

- Tested by the accredited testing institute SKZ
- Hygienically safe in accordance with the KTW guideline of the Federal Environmental Agency
- Compliance with standards according to EN ISO 15874

9.1.2 Testing Institutes for Product Monitoring and Certification

Prüfstelle Wasser


Das Kunststoff-Zentrum

Staatliche Versuchsanstalt

### 9.2 POLO-ECOSAN Letter of Guarantee

## GUARANTEE DECLARATION POLO-ECOSAN

In line with our corporate philosophy, top tube and moulding quality includes the subsequent guarantee for in-company manufactured products from POLOPLAST's POLO-ECOSAN programme. In addition to any legal warranty and damage claims, upon the agreement of POLOPLAST's general terms of business, the company undertakes the following

## GUARANTEE

 dar解 laying and installation instructions, the lack of the characteristics expressly guaranteed by POLOPLAST, or damages caused by POLOPLAST through the use of products covered by this guarantee. This liability shall be valid for a period of $\mathbf{1 0}$ years from the date of manufacture and encompass:

1. The free delivery to the place of employment of the replacement parts required for the repair of the damage, as well as
2. the necessary removal and installation costs, including the expenses incurred for the restoration of the object to its original condition, up to a sum of $€ 2,000,000$ per occurrence of damage.

Pursuant to this declaration POLOPLAST provides this guarantee to its contractual partners when

1. laying was completed by trained personnel from a licensed sanitary plumping company in connection with installation as contractually intended and all the technical regulations valid at the time of completion were observed;
2. the contractual partner proves that only POLOPLAST original parts were employed and that these were not combined with products of any other origin;
3. the contractual partner proves that the cause of damage did not relate to parts subject to natural wear and tear, to external mechanical damage, or other external influences on the product;
4. it can be proven that at the time of laying all the current storage, laying, installation and application stipulations were observed in full;
5. all the measures necessary for damage minimisation were initiated immediately;
6. the occurrence of damage was reported to POLOPAST without delay and under all circumstances within seven days of the identification of the damage, complete with information concerning the related facts and circumstances;
7. prior to repair work, POLOPLAST is given an opportunity to determine and appraise the damage itself or through a third party,
8. all the parts relating to the claim are kept for the investigation of the damage occurrence and are provided to POLOPLAST upon request;
9. the date of production and installation are evidenced in suitable form (pressure test report);
10. the related delivery documents are presented to POLOPLAST.
9.3 POLO-UV ML5 Letter of Guarantee

## GUARANTEE DECLARATION POLO-UV ML5

In line with our corporate philosophy, top tube and moulding quality includes the subsequent guarantee for in-company manufactured products from POLOPLAST's POLO-UV ML5 program. In addition to any legal warranty and damage claims, upon the agreement of POLOPLAST's general terms of business, the company undertakes the following

## GUARANTEE

POLOPLAST assumes for installation under outdoor environments worldwide (with the exception of Areas with higher yearly UV-radiation than usual in Aswan, Egypt) liability for damages, resulting from manufacturing errors, deficiencies caused by incorrect storage, laying and installation instructions, the lack of the characteristics expressly guaranteed by POLOPLAST, or damages caused by POLOPLAST through the use of products covered by this guarantee. This liability shall be valid for a period of $\mathbf{1 0}$ years from the date of manufacture and encompass:

1. The free delivery to the place of employment of the replacement parts required for the repair of the damage, as well as
2. the necessary removal and installation costs, including the expenses incurred for the restoration of the object to its original condition, up to a sum of $€ 2,000,000$ per occurrence of damage.

Pursuant to this declaration POLOPLAST provides this guarantee to its contractual partners when

1. laying was completed by trained personnel from a licensed sanitary plumping company in connection with installation as contractually intended and all the technical regulations valid at the time of completion were observed;
2. the contractual partner proves that only POLOPLAST original parts were employed and that these were not combined with products of any other origin;
3. the contractual partner proves that the cause of damage did not relate to parts subject to natural wear and tear, to external mechanical damage, or other external influences on the product;
4. it can be proven that at the time of laying all the current storage, laying, installation and application stipulations were observed in full;
5. all the measures necessary for damage minimisation were initiated immediately;
6. the occurrence of damage was reported to POLOPAST without delay and under all circumstances within seven days of the identification of the damage, complete with information concerning the related facts and circumstances;
7. prior to repair work, POLOPLAST is given an opportunity to determine and appraise the damage itself or through a third party;
8. all the parts relating to the claim are kept for the investigation of the damage occurrence and are provided to POLOPLAST upon request;
9. the date of production and installation are evidenced in suitable form (pressure test report);
10. the related delivery documents are presented to POLOPLAST.

## QUALITY MANAGEMENT

### 9.4 Sustainability

In the development of its products and their production, POLOPLAST places emphasis on the sustainable, environmentally friendly and resource-conserving implementation. The raw material polypropylene PP-R can be recycled to 100\%. Any residues from the production can be reused.

Thanks to this advantage it can be processed further for the industry in many different ways. Compared to other materials, the energy expenditure required for the production of POLOPLAST products is significantly lower. Furthermore, the process does not produce any environmentally hazardous substances, leading to an excellent environmental performance evaluation overall.

## Advantages PP-R:

- Can be recycled
- Free of halogen
- Free of plasticisers
- Hygienically safe
- Environmentally friendly


NOTES

NOTES

NOTES


[^0]:    POLOPLAST pipes made of PP-R and PP-RCT are manufactured according to DIN EN ISO 15874, EN ISO 21003 and DIN 8077/78 and fulfil their quality requirements.

[^1]:    Send inquiry to: POLOPLAST GmbH
    Kirnachstrasse 17. 87640 Ebenhofen. Germany
    Tel. +49 (0) 8342 . 7006 . 0
    Fax +49 (0) 8342 . 7006.66
    info@poloplast.com . www.poloplast.com

[^2]:    Place
    Date
    Client $\qquad$ Contractor
    1）The pressure gauges used must allow a precise reading of a 1 mbar change in pressure．
    2）The pressure gauges used must allow a precise reading of a 0.1 bar change in pressure．

